



# Unit 3

## Basics of superconductivity

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# Scope of the course



- Basics of superconductivity
  1. History
  2. General principles
  3. Diamagnetism
  4. Type I and II superconductors
  5. Flux pinning and flux creep
  6. Critical surfaces for superconducting materials



# References

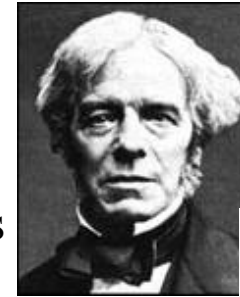


- Wilson, “Superconducting Magnets”
- Mess, Schmueser, Wolff, “Superconducting Accelerator Magnets”
- Arno Godeke, thesis: “Performance Boundaries in Nb<sub>3</sub>Sn Superconductors”
- Alex Guerivich, Lectures on Superconductivity
- Roberto Casalbuoni: Lecture Notes on Superconductivity: Condensed Matter and QCD



## Cryogenics is the science of producing temperatures below ~200K

- Faraday (~1820's) demonstrates ability to liquify most known gases by first cooling with a bath of ether and dry ice, followed by pressurization
  - he was unable to liquify oxygen, hydrogen, nitrogen, carbon monoxide, methane, and nitric oxide
  - The noble gases, helium, argon, neon, krypton and xenon had not yet been discovered (many of these are critical cryogenic fluids today)
- In 1848 Lord Kelvin determined the existence of absolute zero:
  - $0K = -273C (= -459F)$
- In 1877 Louis Cailletet (France) and Raoul-Pierre Pictet (Switzerland) succeed in liquifying air
- In 1883 Von Wroblewski (Cracow) succeeds in liquifying Oxygen
- In 1898 James Dewar succeeded in liquifying hydrogen (~20K!); he then went on to freeze hydrogen (14K).
- Helium remained elusive; it was first discovered in the spectrum of the sun
- 1908: Kamerlingh Onnes succeeded in liquifying Helium





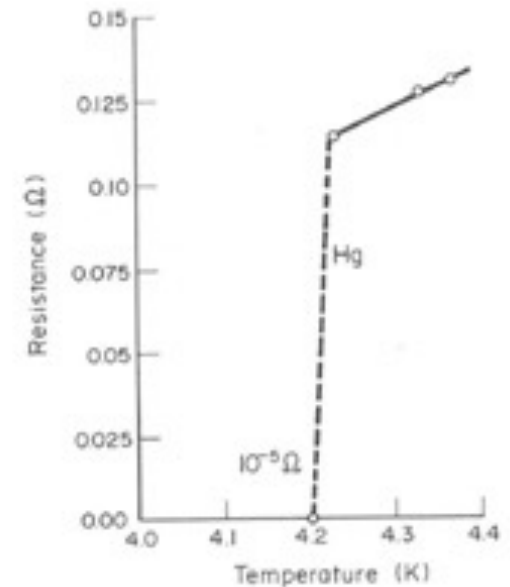
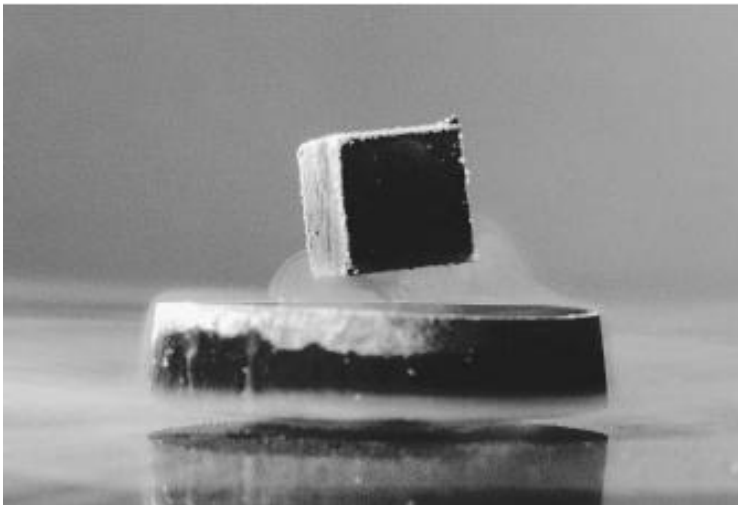


# History

- 1911: Kamerlingh Onnes discovery of mercury superconductivity: “Perfect conductors”
  - A few years earlier he had succeeded in liquifying Helium, a critical technological feat needed for the discovery
- 1933: Meissner and Ochsenfeld discover perfect *diamagnetic* characteristic of superconductivity



Kamerlingh Onnes,  
Nobel Prize 1913





- A theory of superconductivity took time to evolve:
  - 1935: London brothers propose two equations for E and H
    - results in concept of penetration depth  $\lambda$
  - 1950: Ginzburg and Landau propose a macroscopic theory (GL) for superconductivity, based on Landau's theory of second-order phase transitions
    - Results in concept of coherence length  $\xi$



Heinz and Fritz London



Ginzburg and Landau (circa 1947)  
Nobel Prize 2003: Ginzburg, Abrikosov, Leggett



# History - theory

- 1957: Bardeen, Cooper, and Schrieffer publish microscopic theory (BCS) of Cooper-pair formation that continues to be held as the standard for low-temperature superconductors
- 1957: Abrikosov considered GL theory for case  $\kappa=\lambda/\epsilon \gg 1$ 
  - Introduced concept of Type II superconductor
  - Predicted flux penetrates in fixed quanta, in the form of a vortex array



Bardeen, Cooper and Schrieffer  
Nobel Prize 1972



# History - theory

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*Nobel Prize 2003: Ginzburg, Abrikosov, Leggett (the GLAG members)*



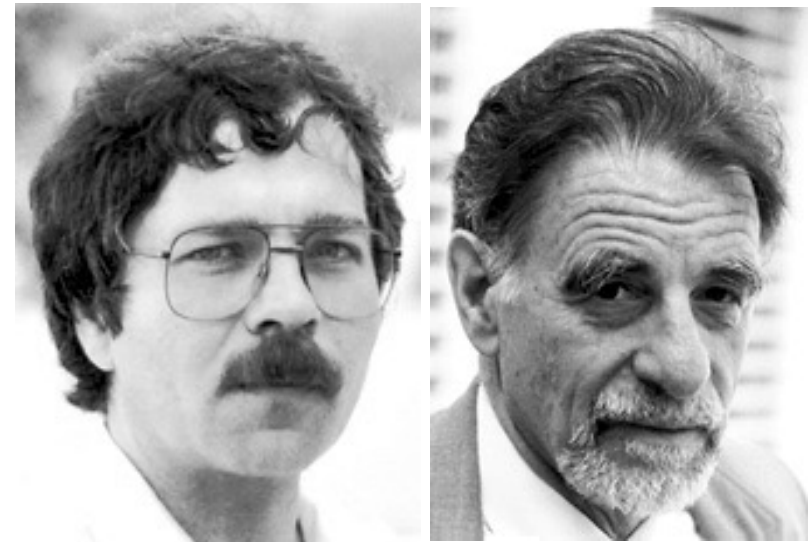
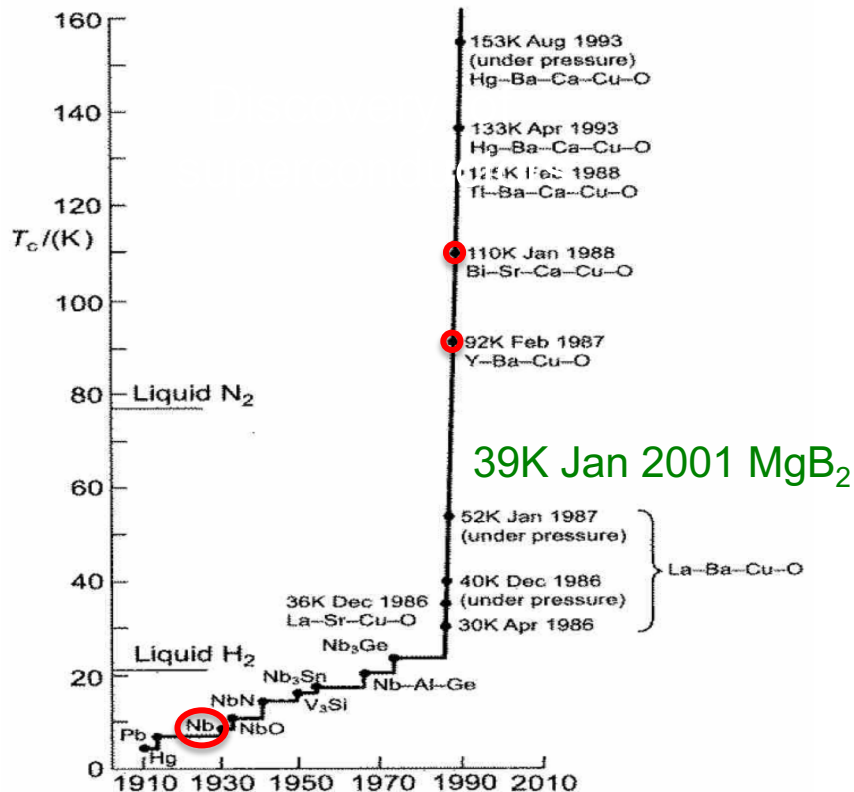
Abrikosov with Princess Madeleine



# History – High temperature superconductors



- 1986: Bednorz and Muller discover superconductivity at high temperatures in layered materials comprising copper oxide planes



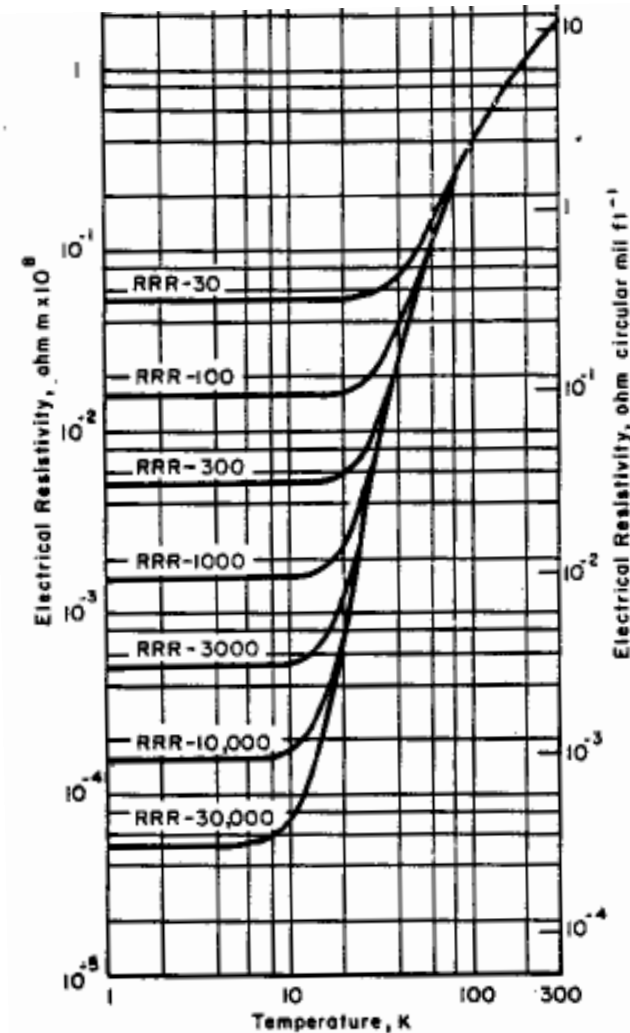
George Bednorz and Alexander Muller  
Nobel prize for Physics (1987)





# General Principals

- Superconductivity refers to a material state in which current can flow with no resistance
  - Not just “little” resistance - truly ZERO resistance
  - Resistance in a conductor stems from scattering of electrons off of thermally activated ions
    - Resistance therefore goes down as temperature decreases
    - The decrease in resistance in normal metals reaches a minimum based on irregularities and impurities in the lattice, hence concept of RRR (Residual resistivity ratio)
  - RRR is a rough measure of cold-work and impurities in a metal



$$RRR = \rho(273K) / \rho(4K)$$



# Aside: Maxwell's equations

$$\nabla \cdot \vec{E} = \frac{\rho}{\epsilon} \quad \text{Gauss' law}$$

$$\nabla \cdot \vec{B} = 0$$

$$\nabla \times \vec{E} = -\frac{\partial \vec{B}}{\partial t} \quad \text{Faraday's law}$$

$$\nabla \times \vec{B} = \mu_0 \vec{J} + \mu_0 \epsilon_0 \frac{\partial \vec{E}}{\partial t} \quad \text{Ampere's law (corrected by Maxwell)}$$

$$\mu_0 = 4\pi \times 10^{-7} \quad N/A^2 \quad \text{Permeability of free space}$$

$$\epsilon_0 = 8.85 \times 10^{-12} \quad C^2/(Nm^2) \quad \text{Permittivity of free space}$$



# Some reminders of useful formulas



$$\nabla \cdot (\nabla \times \bar{F}) = 0 \quad \forall \bar{F} \qquad \nabla \times (\nabla \times \bar{F}) = \nabla(\nabla \cdot \bar{F}) - \nabla^2 \bar{F} \quad \forall \bar{F}$$

$$\nabla \times (\nabla u) = 0 \quad \forall u \qquad \text{or} \qquad \nabla \times \bar{F} = 0 \quad \Leftrightarrow \quad \bar{F} = \nabla u$$

( $F$  is conservative if curl  $F$  is zero)

$$\int_S \bar{F} \cdot \bar{n} \, dS = \int_V \nabla \cdot \bar{F} \, dV$$

Volume Integral

Divergence Theorem

$$\oint_l \bar{F} \cdot d\bar{l} = \int_S (\nabla \times \bar{F}) \cdot \bar{n} \, dS$$

Surface Integral (Flux)

Curl Theorem (Stoke's Theorem)

Line Integral (Circulation)





# Some direct results from Maxwell

- Electric and magnetic fields are fundamentally linked
  - $dB/dt$  induces voltage (Faraday)
  - Moving charge generates B (Ampere)
- Amperes law applied to DC fields and flowing currents:

$$\nabla \times \vec{B} = \mu_0 \vec{J} \Rightarrow \oint \vec{B} \cdot d\vec{l} = \mu_0 I_{enclosed}$$

- Gauss's law: no magnetic monopoles

$$\nabla \cdot \vec{B} = 0$$

*Magnetic field lines cannot emanate from a point; they "curl" around current*

- Equations admit wave solutions
  - Take the curl of Faraday's and Ampere's laws; E and B admit waves with velocity

$$v = \sqrt{\frac{1}{\mu_0 \epsilon}} = c = \text{speed of light}$$



# Magnetization

- From a macroscopic perspective, critical insight can be gleaned from magnetization measurements
  - Magnetization is the magnetic (dipole) moment generated in a material by an applied field

$$\nabla \times B = \mu_0 J$$

*Amperes law*

$$J = J_{free} + J_{bound}$$

$$J_{bound} = \nabla \times M$$

*Arbitrary but useful distinction*

$$\Rightarrow H = \frac{1}{\mu_0} B - M$$

*Results in a practical definition: we know and control free currents*

$$\Rightarrow \nabla \times H = J_{free} \Rightarrow \oint H \cdot dl = I_{enclosed \text{ free current}}$$

Note:  
We do not *need* M; every calculation could be performed using B and H



# magnetization in superconductors

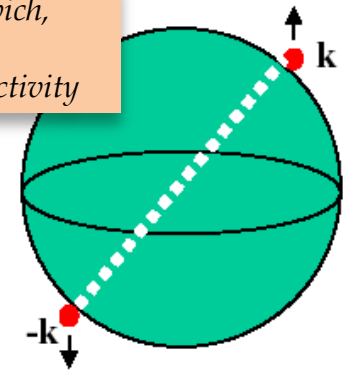
- Example: iron is ferromagnetic – it has a strong paramagnetic moment (i.e. the magnetization is parallel and additive to the applied field)
  - Most materials are either diamagnetic or paramagnetic, but the moments are extremely small compared to ferromagnetism
  - In diamagnetic and paramagnetic materials, the magnetization is a function of the applied field, i.e. remove the field, and the magnetization disappears.
  - In ferromagnetic materials, some of the magnetization remains “frozen in” => hysteretic behavior





# Basics of superconductivity

Alex Guerivich,  
lecture on  
superconductivity



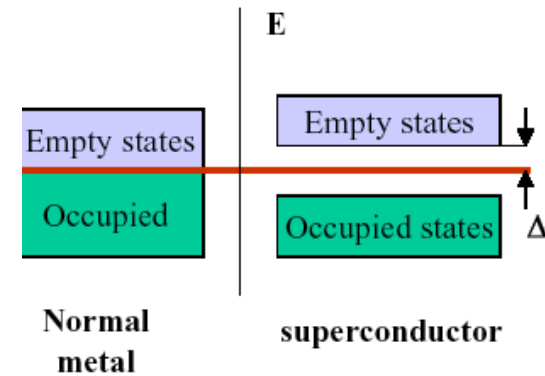
Cooper pair on the Fermi surface

• In a superconductor, when the temperature descends below the critical temperature, electrons find it energetically preferable to form Cooper pairs

- The Cooper pairs interact with the positive ions of the lattice
- Lattice vibrations are often termed “phonons”; hence the coupling between the electron-pair and the lattice is referred to as electron-phonon interaction
- The balance between electron-phonon interaction forces and Coulomb (electrostatic) forces determines if a given material is superconducting

Electron-phonon interaction can occur over long distances; Cooper pairs can be separated by many lattice spacings

**BCS breakthrough:**  
Fermi surface is unstable to bound states of electron-pairs

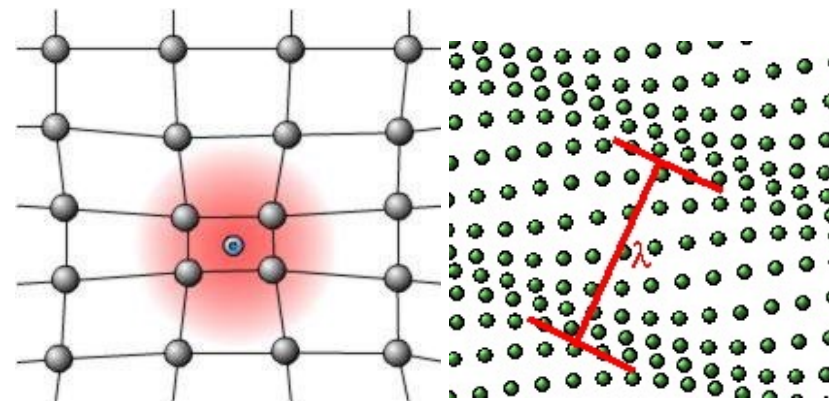


$\sim meV \sim 10^{-22} J!!$

$$\Delta_0 \cong 2\hbar\omega_D \exp\left[-\frac{1}{\lambda_{ep}}\right]$$

$$T_c \cong \frac{e^\gamma}{\pi k_b} \Delta_0$$

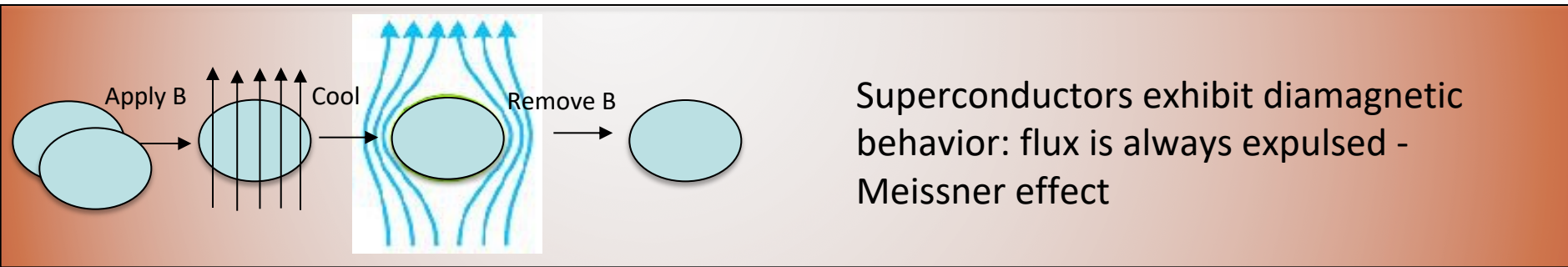
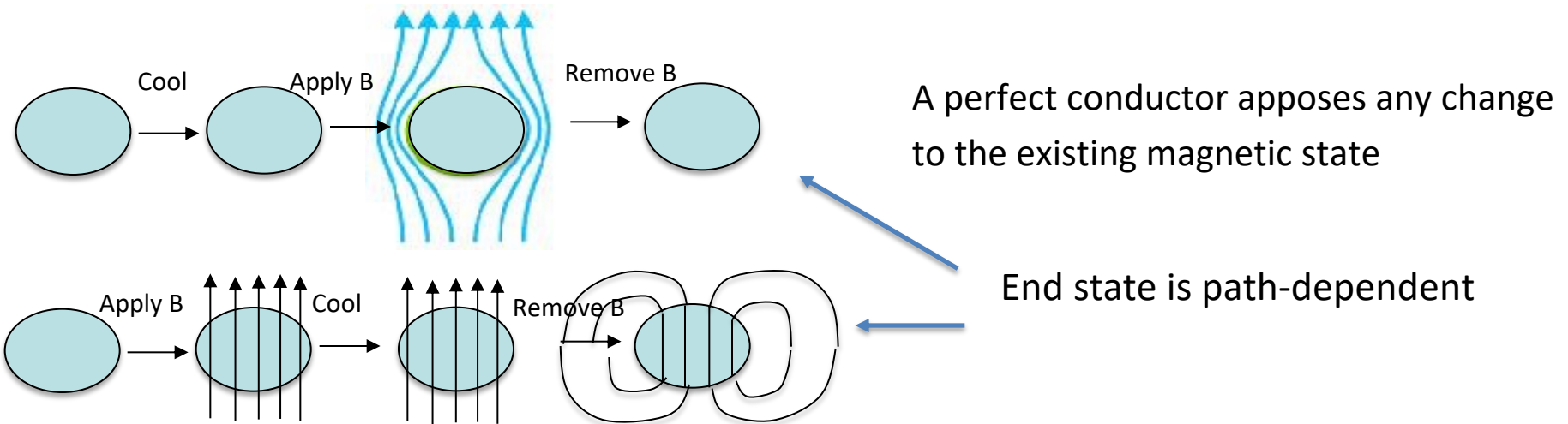
$k_B$ =Boltzmann constant =  $1.38 \times 10^{-23}$   
 $\omega_D$ =Debye frequency  
 $\lambda_{ep}$ =electron-phonon coupling  
 $\gamma$ =euler constant=0.577





# Diamagnetic behavior of superconductors

- What differentiates a “perfect” conductor from a diamagnetic material?





# The London equations

- Derive starting from the classical Drude model, but adapt to account for the Meissner effect:
  - The Drude model of solid state physics applies classical kinetics to electron motion
    - ✓ Assumes static positively charged nucleus, electron gas of density  $n$ .
    - ✓ Electron motion damped by collisions

$$\begin{aligned} m \frac{d\vec{v}}{dt} &= e\vec{E} - \gamma\vec{v} \quad \leftarrow \text{“Frictional drag” on “normal” conduction electrons} \\ \vec{J}_s &= -en_s\vec{v} \\ \Rightarrow \frac{\partial}{\partial t} \left( \frac{m}{n_s e^2} \nabla \times \vec{J}_s + \vec{B} \right) &= 0 \implies \nabla^2 \vec{B} = \frac{\mu_0 n_s e^2}{m} \vec{B} = \frac{1}{\lambda_L^2} \vec{B} \end{aligned}$$

- The penetration depth  $\lambda_L$  is the characteristic depth of the supercurrents on the surface of the material.



# Concept of coherence length

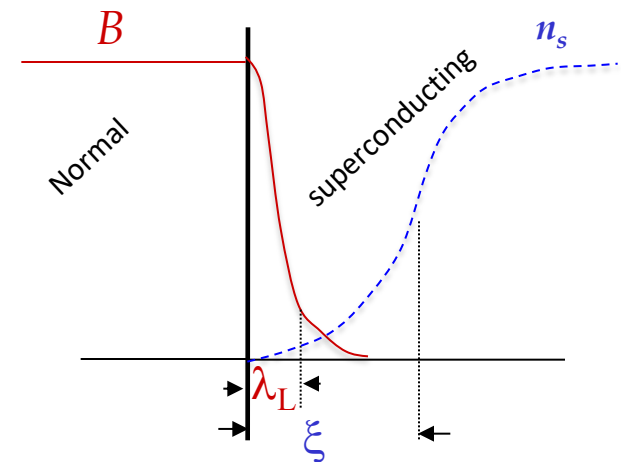
- The density of superconducting electrons  $n_s$  decreases to zero near a superconducting / normal interface, with a characteristic length  $\xi$  (coherence length, first introduced by Pippard in 1953). The two length scales  $\xi$  and  $\lambda_L$  define much of the superconductors behavior.
  - The coherence length is proportional to the mean free path of conduction electrons; e.g. for pure metals it is quite large, but for alloys (and ceramics...) it is often very small. Their ratio, the GL parameter, determines flux penetration:

- From “GLAG” theory, if: 
$$\kappa = \lambda_L / \xi$$

$\kappa < 1/\sqrt{2}$  Type I superconductor

$\kappa > 1/\sqrt{2}$  Type II superconductor

*Note: in reality  $\xi$  and  $\lambda_L$  are functions of temperature*







# Thermodynamic critical field

- The Gibbs free energy of the superconducting state is lower than the normal state. As the applied field  $B$  increases, the Gibbs free energy increases by  $B^2/2\mu_0$ .
- The thermodynamic critical field at  $T=0$  corresponds to the balancing of the superconducting and normal Gibbs energies:

$$G_n = G_s + \frac{H_c^2}{2\mu_0}$$

- The BCS theory states that  $H_c(0)$  can be calculated from the electronic specific heat (Sommerfeld coefficient):

$$H_c(0) = 7.65 \times 10^{-4} \frac{\gamma^{1/2} T_c}{\mu_0}$$

**Table 2.2. Coefficient of the Electronic Specific Heat for Various Metallic Elements of Technical Interest<sup>a</sup>**

Element	$\gamma$ (mJ/mol · K <sup>2</sup> )
Ag	0.646
Al	1.35
Au	0.729
Cd	0.688
Cr	1.40
Cu	0.695
Fe	4.98
Ga	0.596
Hf	2.16
Hg	1.79
In	1.69
Nb	7.79
Ni	7.02
Pb	2.98
Sn	1.78
Ti	3.35
V	9.26
Zn	0.64
Zr	2.80

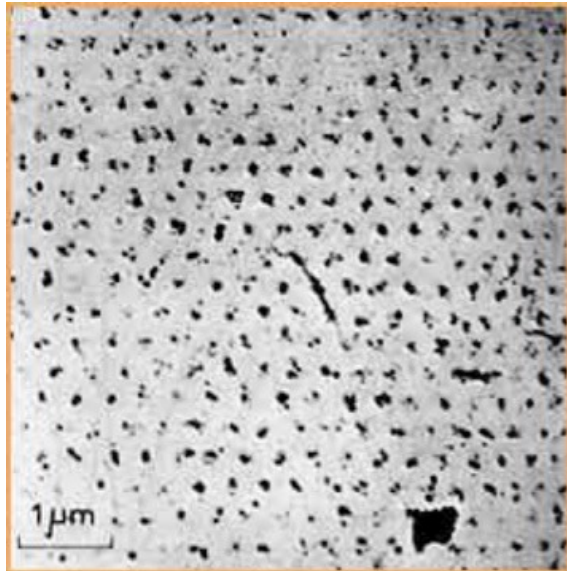
<sup>a</sup> From Kittel!





# Type I and II superconductors

- Type I superconductors are characterized by the Meissner effect, i.e. flux is fully expelled through the existence of supercurrents over a distance  $\lambda_L$ .
- Type II superconductors find it energetically favorable to allow flux to enter via normal zones of fixed flux quanta: “fluxoids” or vortices.
  - The fluxoids or flux lines are vortices of normal material of size  $\sim \pi \xi^2$  “surrounded” by supercurrents shielding the superconducting material.



*First photograph of vortex lattice,  
U. Essmann and H. Trauble  
Max-Planck Institute, Stuttgart  
Physics Letters 24A, 526 (1967)*



# Fluxoids



- Fluxoids, or flux lines, are continuous thin tubes characterized by a normal core and shielding supercurrents.
- The flux contained in a fluxoid is quantized:

$$\phi_0 = h/(2e)$$

$$h = \text{Planck's constant} = 6.62607 \times 10^{-34} \text{ Js}$$

$$e = \text{electron charge} = 1.6022 \times 10^{-19} \text{ C}$$

- The fluxoids in an idealized material are uniformly distributed in a triangular lattice so as to minimize the energy state
- Fluxoids in the presence of current flow (e.g. transport current) are subjected to Lorentz force:

$$\vec{F}_L = \vec{J} \times \vec{B}$$

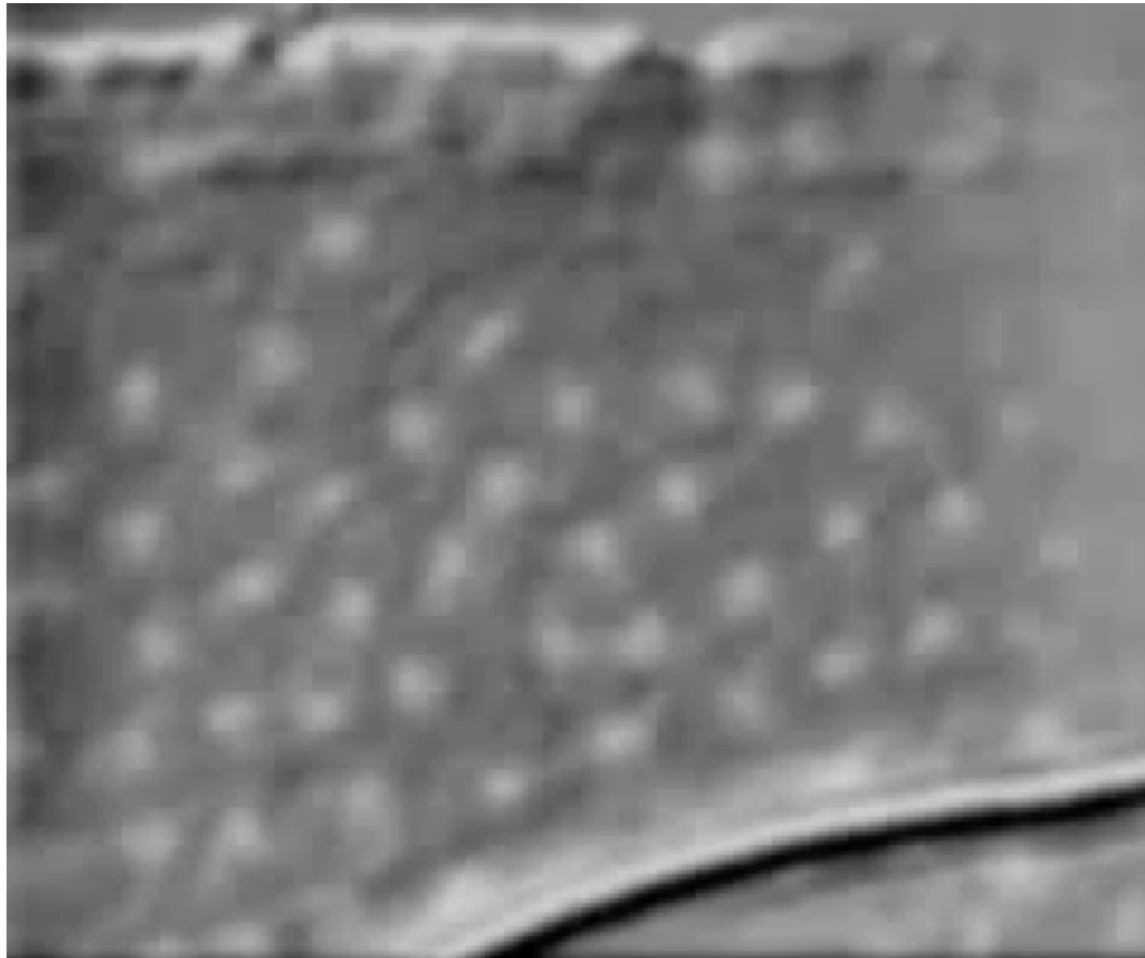
⇒ Concept of flux-flow and associated heating

Solution for real conductors: provide mechanism to *pin* the fluxoids

*See flux flow movies...*



# Visual demonstration of vortices



Penetration of vortices into a superconductor: real-time magneto-optical movie. Each vortex carries one quantum of magnetic flux and is seen as a bright dot. After cooling in a low magnetic field, the field is ramped and vortices slowly enter the superconductor from the edge (located at the top). At larger fields the surface barrier is broken and many vortices penetrate very fast. Movie window: 25x35 microns, sample: NbSe<sub>2</sub> crystal, Lab: University of Oslo. More details: <http://www.fys.uio.no/super/results/sv>



# Critical field definitions

## T=0

- $H_{c1}$ : critical field defining the transition from the Meissner state

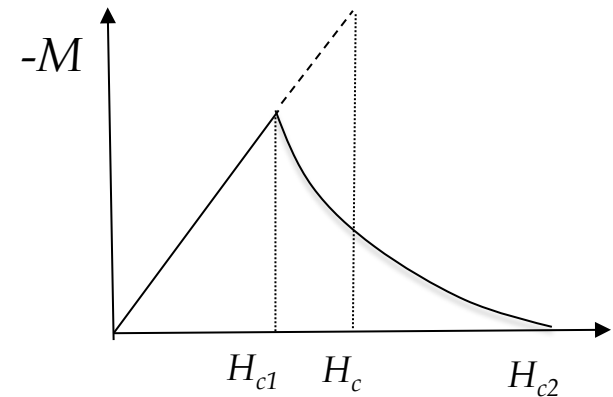
$$H_{c1} \approx \frac{\Phi_0}{4\sqrt{2}\pi\mu_0\lambda^2} \text{Ln}\left(\kappa + \frac{1}{2}\right); \quad \kappa \gg 1$$

- $H_c$ : Thermodynamic critical field
  - $H_c=H_{c1}$  for type I superconductors

$$H_c = \frac{\Phi_0}{2\sqrt{2}\mu_0\kappa\pi\xi^2}$$

- $H_{c2}$ : Critical field defining the transition to the normal state

$$H_{c2} = \frac{\Phi_0}{2\pi\mu_0\xi^2}$$





# Examples of Superconductors

- Many elements are superconducting at sufficiently low temperatures
- None of the pure elements are useful for applications involving transport current, i.e. they do not allow flux penetration
- Superconductors for transport applications are characterized by alloy/composite materials with  $\kappa \gg 1$

Material	$T_c$ (K)	$\lambda(0)$ , nm	$\xi(0)$ , nm	$H_{c2}$ (T)
Nb-Ti	9.5	240	4	13
Nb-N	16	200	5	15
Nb <sub>3</sub> Sn	18	65	3	30
MgB <sub>2</sub> (dirty)	32-39	140	6	35
YBa <sub>2</sub> Cu <sub>3</sub> O <sub>7</sub>	92	150	1.5	>100
Bi-2223	108	200	1.5	>100

Table 2.9. Critical Temperature and Critical Field of Type I Superconductors

Material	$T_c$ (K)	$\mu_0 H_0$ (mT)
Aluminum	1.2	9.9
Cadmium	0.52	3.0
Gallium	1.1	5.1
Indium	3.4	27.6
Iridium	0.11	1.6
Lanthanum $\alpha$	4.8	
$\beta$	4.9	
Lead	7.2	80.3
Lutecium	0.1	35.0
Mercury $\alpha$	4.2	41.3
$\beta$	4.0	34.0
Molybdenum	0.9	
Osmium	0.7	~6.3
Rhenium	1.7	20.1
Rhodium	0.0003	4.9
Ruthenium	0.5	6.6
Tantalum	4.5	83.0
Thalium	2.4	17.1
Thorium	1.4	16.2
Tin	3.7	30.6
Titanium	0.4	
Tungsten	0.016	0.12
Uranium $\alpha$	0.6	
$\beta$	1.8	
Zinc	0.9	5.3
Zirconium	0.8	4.7

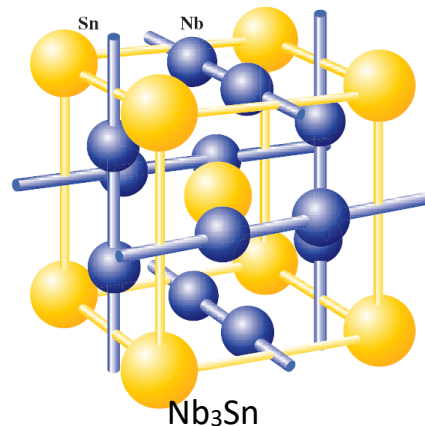


# LTS vs High-Temperature superconductors

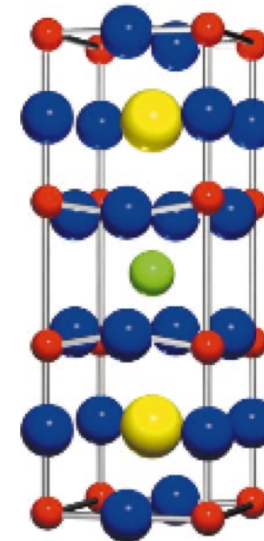
- Much of HTS behavior can be understood in terms of the BCS and GLAG theory parameters
  - The new features of HTS have to do with:
    - 1) highly two-dimensional domains of superconductor, separated by regions of “inert” material
      - Macroscopic behavior is therefore highly anisotropic
      - Different layers must communicate (electrically) via tunneling, or incur Joule losses
    - 2) a much larger range of parameter space in which multiple effects compete
      - The coherence lengths for HTS materials are far smaller than for LTS materials
      - Critical fields are  $\sim 10$  times higher
- => Thermal excitations play a much larger role in HTS behavior



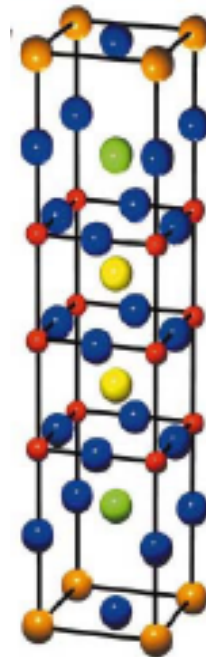
NbTi



Nb<sub>3</sub>Sn



YBCO



BSCCO2223



# Aside – uses for type I superconductors

- Although type I superconductors cannot serve for large-scale transport current applications, they can be used for a variety of applications
  - Excellent electromagnetic shielding for sensitive sensors (e.g. lead can shield a sensor from external EM noise at liquid He temperatures)
  - Niobium can be deposited on a wafer using lithography techniques to develop ultra-sensitive sensors, e.g. transition-edge sensors
    - Using a bias voltage and Joule heating, the superconducting material is held at its transition temperature;
    - absorption of a photon changes the circuit resistance and hence the transport current, which can then be detected with a SQUID (superconducting quantum interference device)

See for example research by J. Clarke, UC

Berkeley;

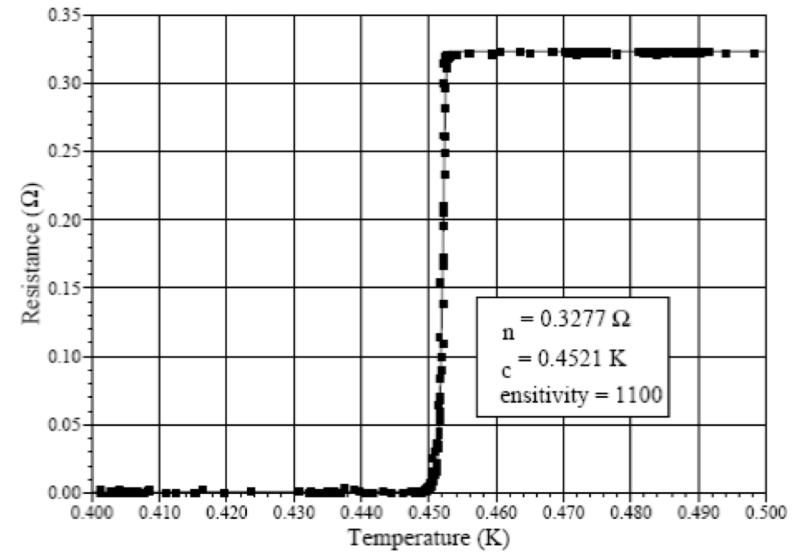


Figure 2. Resistance vs. temperature for a high-sensitivity TES bilayer.

*Mo/Au bilayer TES detector*

*Courtesy Benford and Moseley, NASA Goddard*





# Flux Flow

- The Lorentz force acting on a fluxoid will, in the absence of pinning, result in motion of the fluxoid
- Fluxoid motion generates a potential gradient (i.e. voltage) and hence heating
  - This can be modeled using Faraday's law of induction:

$$\vec{E} = \vec{B} \times \vec{v}_f \quad \text{Lorentz force}$$
$$\text{Work done } \dot{w} = nF_L \cdot \vec{v}_f = (\vec{J} \times \vec{B}) \cdot \vec{v}_L = \vec{J} \cdot \vec{E} = JE$$
$$\boxed{\vec{E} = \rho_{ff} \vec{J}} \quad \text{"Flux-flow resistivity"}$$

⇒ *"ideal" superconductors can support no transport current beyond  $H_{c1}$ !*

- Real superconductors have defects that can prevent the flow of fluxoids
  - The ability of real conductors to carry transport current depends on the number, distribution, and strength of such pinning centers





# Flux pinning

- Fluxoids can be pinned by a wide variety of material defects
  - Inclusions
    - Under certain conditions, small inclusions of appropriate materials can serve as pinning site locations; this suggests tailoring the material artificially through manufacturing
  - Lattice dislocations / grain boundaries
    - These are known to be primary pinning sites. Superconductor materials for wires are severely work hardened so as to maximize the number and distribution of grain boundaries.
  - Precipitation of other material phases
    - In NbTi, mild heat treatment can lead to the precipitation of an  $\alpha$ -phase Ti-rich alloy that provides excellent pinning strength.

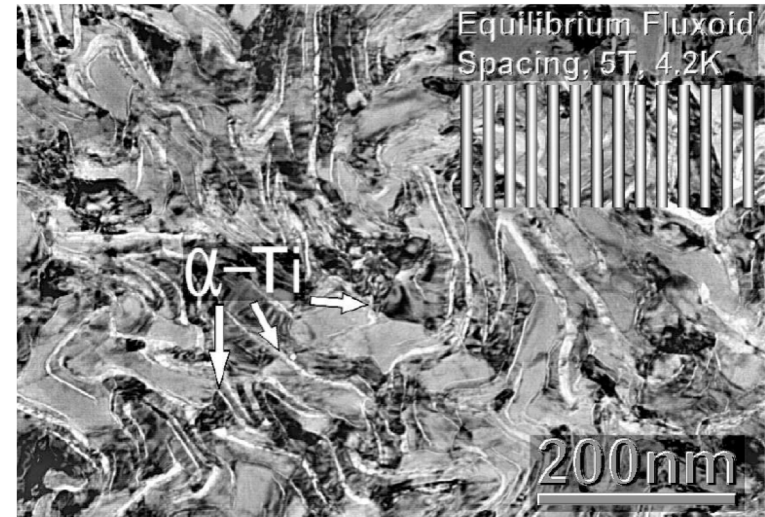


Fig. 1: Microstructure of a NbTi filament (Courtesy of P.J. Lee, University of Wisconsin at Madison).

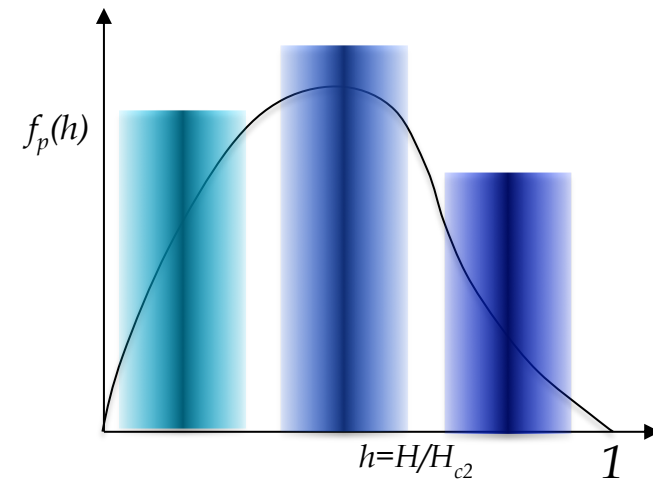


Fig. 6: Microstructure of a Nb<sub>3</sub>Sn filament (Courtesy of C. Verwaerde, Alstom/MSA).



# Pinning strength

- The distribution and pinning of fluxoids depends on the operating regime:
  - At low field (but  $> H_{c1}$ ) the distribution is governed mainly by interaction between flux-lines, i.e. the fluxoids find it energetically advantageous to distribute themselves “evenly” over the volume (rather weak)
  - At intermediate fields, the pinning force is provided by the pinning sites, capable of hindering flux flow by withstanding the Lorentz force acting on the fluxoids. Ideally, the pinning sites are uniformly distributed in the material (very strong)
  - At high field, the number of fluxoids significantly exceeds the number of pinning sites; the effective pinning strength is a combination of defect pinning strength and shear strength of the fluxlines (rather weak)





# Modeling pinning

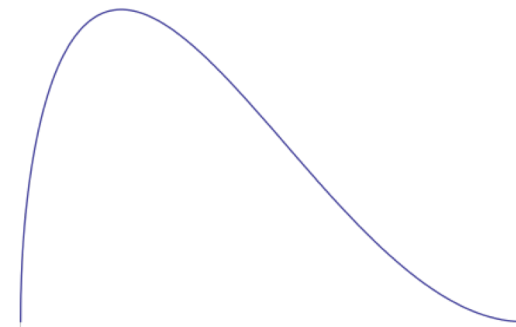
- Precise first-principles physical descriptions of overall pinning strength (and hence critical current) of real superconductors is difficult due to ambiguities intrinsic in pinning
- Nevertheless, models based on sound physics minimize free parameters needed to fit measured data and provide reliable estimates for classes of materials
- One of the most cited correlations is that of Kramer:

$$F_p = F_{\max} f(h) \propto \frac{H^\nu}{\kappa^\gamma} f(h)$$

$$f(h) = h^{1/2} (1-h)^2; \quad h = H / H_{c2}$$

The fitting coefficients  $\nu$  and  $\gamma$  depend on the type of pinning. Furthermore, it is experimentally verified that

$$H_c(T) \approx H_c(0) \left[ 1 - \left( \frac{T}{T_c} \right)^2 \right]$$

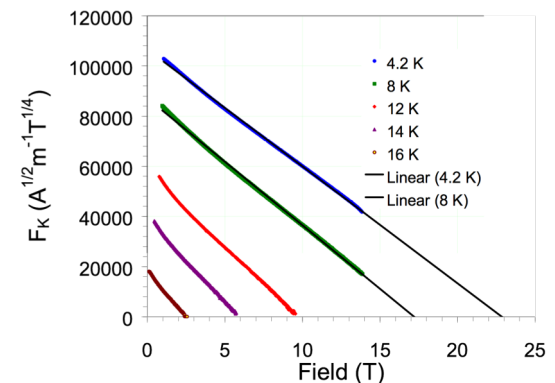


**“Kramer plot”**

$$F_p = J_c B \propto b^{1/2} (1-b)^2$$

$$F_K = J_c^{1/2} B^{1/4} \propto (1-b)$$

From L. Cooley, USPAS





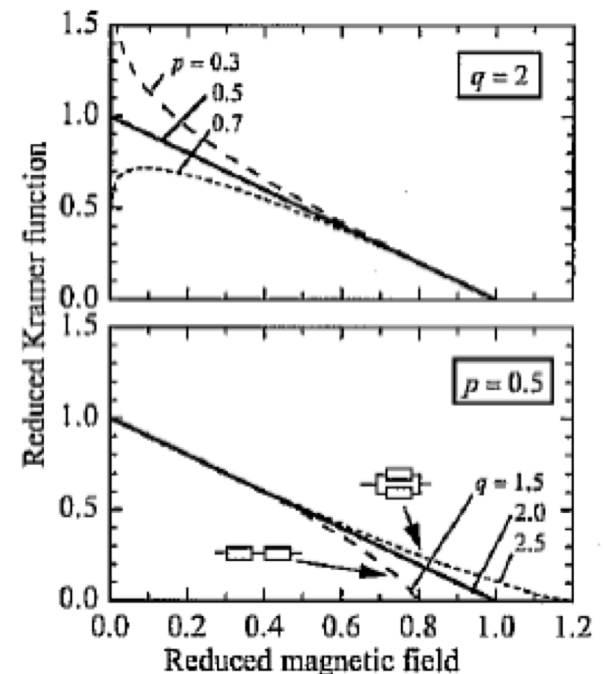
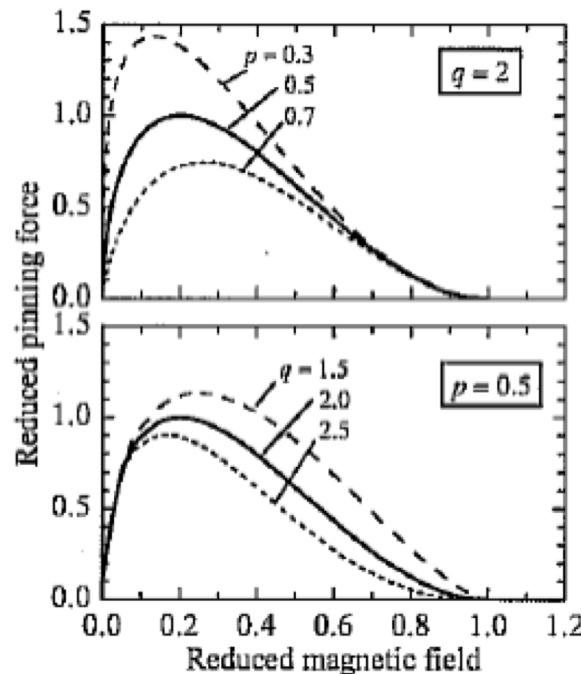
# Scaling of critical current: field dependence

- The Kramer formulation provides excellent fits in the region  $0.2 < h < 0.6$  for  $Nb_3Sn$ ; it is appropriate for regimes where the number of fluxoids exceeds the number of pinning sites
- Outside this region, a variety of effects (e.g. inhomogeneity averaging) can alter the pinning strength behavior, so the pinning strength is often fitted with the generalization

$$f_p(h) \propto h^p (1-h)^q; \quad h = H / H_{c2}$$

- It is preferable to stay with the Kramer formulation, yielding:

$$J_c^{1/2} B^{1/4} \simeq \frac{1.1 \times 10^5}{\kappa} \mu_0 (H_{c2} - H)$$





# Scaling of critical current, Nb<sub>3</sub>Sn

## Empirical Strain dependence

- The critical current of Nb<sub>3</sub>Sn is strain dependent, particularly at high field
- The strain dependence is typically modeled in terms of the normalized critical temperature:

$$\frac{H_{c2}(4.2, \varepsilon)}{H_{c2m}(0)} \simeq \left[ \frac{T_c(\varepsilon)}{T_{cm}} \right]^3 = s(\varepsilon)$$

- The term  $T_{cm}$  and  $H_{c2m}$  refer to the peaks of the strain-dependent curves
- A “simple” strain model proposed by Ekin yields

$$s(\varepsilon) = 1 - a \left| \varepsilon_{axial} \right|^{1.7}$$
$$a = \begin{cases} 900 & \varepsilon_{axial} < 0 \\ 1250 & \varepsilon_{axial} > 0 \end{cases}$$



# Strain dependence of $J_c$ in $Nb_3Sn$ : physics-based model

- A physics-based model of strain dependence has been developed using the frequency-dependent electron-phonon coupling interactions (Eliashberg; Godeke, Markiewitz)

$$\lambda_{ep}(\varepsilon) = 2 \int \frac{\alpha^2(\omega) F(\omega)}{\omega} d\omega$$

*Phonon density of states*  $\nearrow$

- From the interaction parameter the strain dependence of  $T_c$  can be derived
- Experimentally, the strain dependence of  $H_{c2}$  behaves as

$$\frac{H_{c2}(4.2, \varepsilon)}{H_{c2m}(4.2)} \cong \frac{T_c(\varepsilon)}{T_{cm}}$$

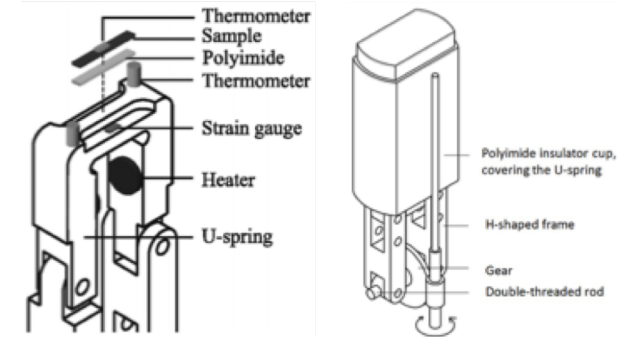
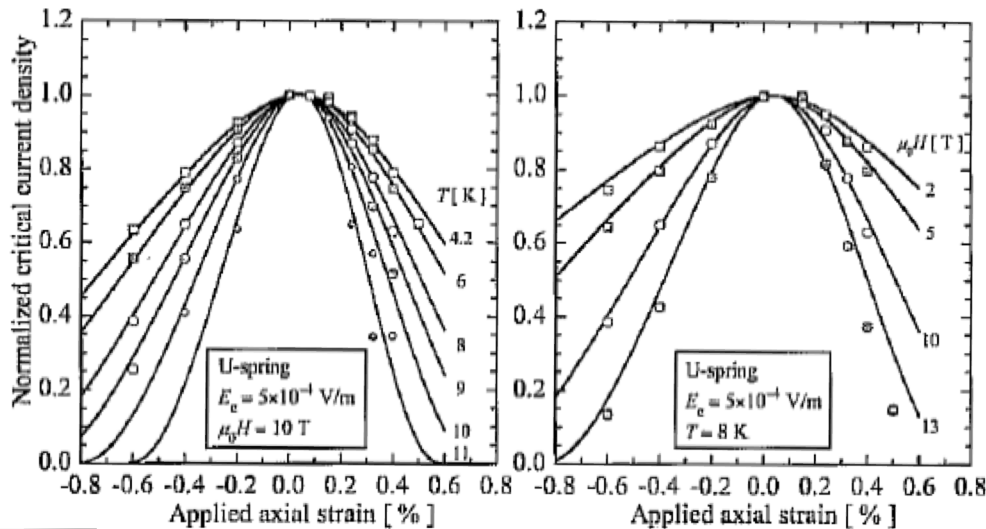
- The theory predicts strain dependence of  $J_c$  for all LTS materials, but the amplitude of the strain effects varies (e.g. very small for NbTi)
- The resulting model describes quite well the asymmetry in the strain dependence of  $B_{c2}$ , and the experimentally observed strong dependence on the deviatoric strain



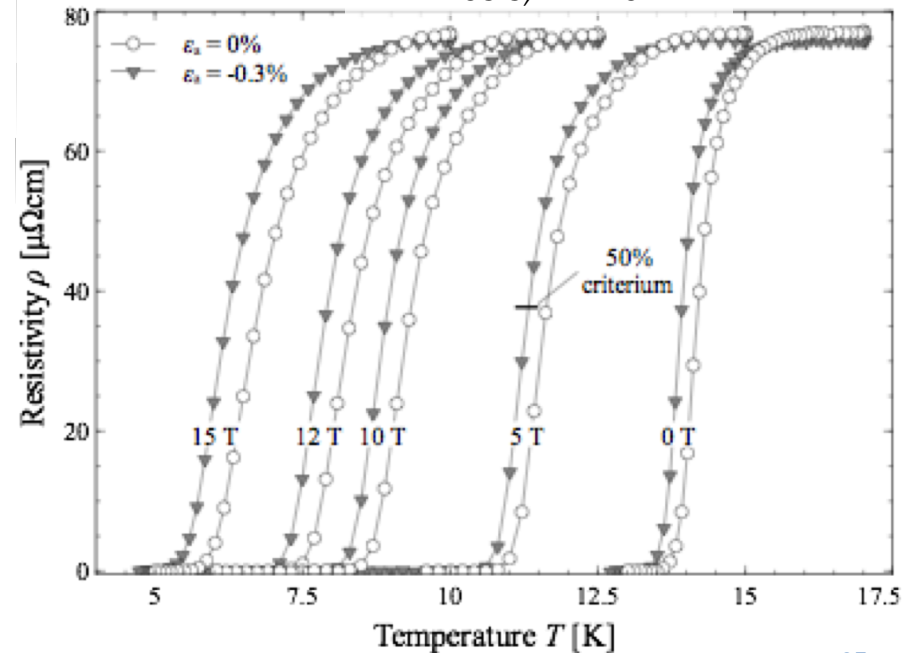


# Strain dependence of $J_c$ in $Nb_3Sn$

- The strain dependence is a strong function of the applied field and of temperature



PhD thesis, M. Mentink





# Critical surface: Example fit for NbTi

- NbTi parameterization

- Temperature dependence of  $B_{C2}$  is provided by Lubell's formulae:

$$B_{C2}(T) = B_{C20} \left[ 1 - \left( \frac{T}{T_{C0}} \right)^{1.7} \right]$$

where  $B_{C20}$  is the upper critical flux density at zero temperature ( $\sim 14.5$  T)

- Temperature and field dependence of  $J_c$  can be modeled, for example, by Bottura's formula

$$\frac{J_c(B, T)}{J_{C,ref}} = \frac{C_{NbTi}}{B} \left[ \frac{B}{B_{C2}(T)} \right]^{\alpha_{NbTi}} \left[ 1 - \frac{B}{B_{C2}(T)} \right]^{\beta_{NbTi}} \left[ 1 - \left( \frac{T}{T_{C0}} \right)^{1.7} \right]^{\gamma_{NbTi}}$$

where  $J_{C,Ref}$  is critical current density at 4.2 K and 5 T (e.g.  $\sim 3000$  A/mm<sup>2</sup>) and  $C_{NbTi}$  ( $\sim 30$  T),  $\alpha_{NbTi}$  ( $\sim 0.6$ ),  $\beta_{NbTi}$  ( $\sim 1.0$ ), and  $\gamma_{NbTi}$  ( $\sim 2.3$ ) are fitting parameters.





# Scaling $J_c$ for NbTi & Nb<sub>3</sub>Sn

(Courtesy Arno Godeke)



$$J_c(H, T, \varepsilon) \equiv \frac{C_1}{\mu_0 H} s(\varepsilon) \underbrace{(1 - t^{n_1})(1 - t^{n_2})}_{\text{fits for NbTi}} h^p (1 - h)^q,$$

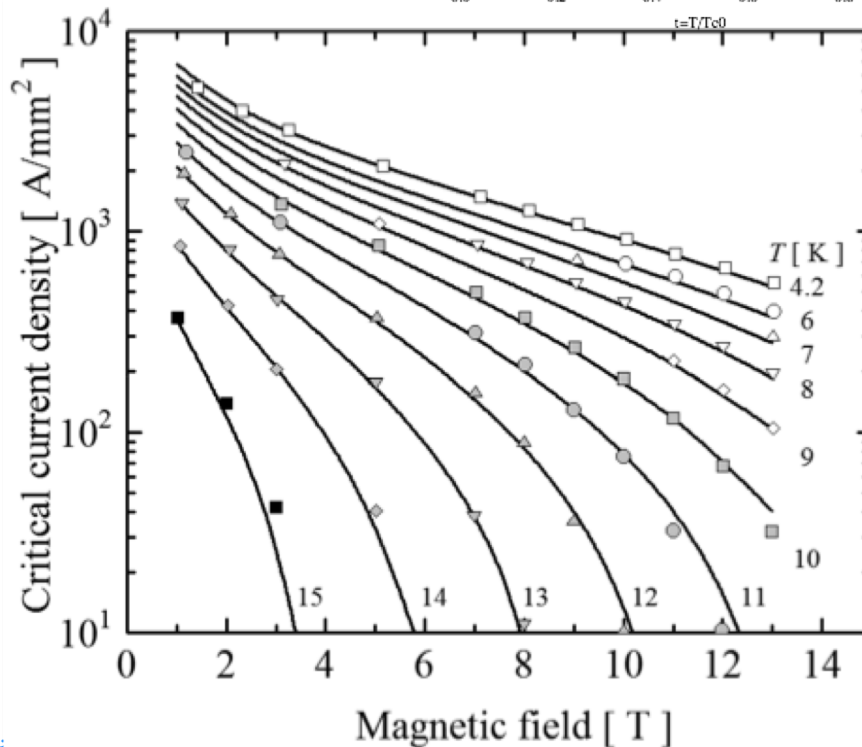
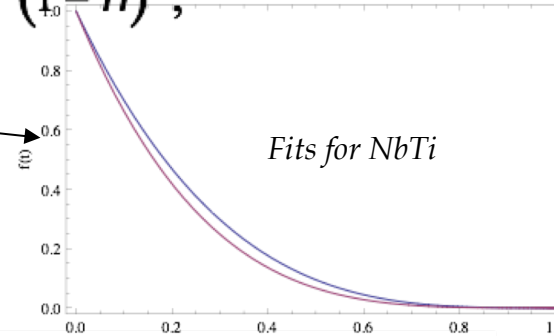
with

$$t \equiv T/T_c^*(\varepsilon), \quad h \equiv H/H_{c2}^*(T, \varepsilon),$$

$$H_{c2}^*(T, \varepsilon) \equiv H_{c2m}^*(0) s(\varepsilon) (1 - t^{n_1}),$$

$$T_c^*(\varepsilon) = T_{cm}^* s(\varepsilon)^{\frac{1}{3}}$$

Godeke et al.,  
SUST 19 (2006)



## Nb<sub>3</sub>Sn

Godeke, SuST 19

- $n_1 \approx 1.52$
- $n_2 = 2$
- $p = 0.5$
- $q = 2$
- $s(\varepsilon) = \text{strain dependence}$

## NbTi

Bottura, TAS 19

- $n_1 = n_2 \approx 1.7$
- $p \approx 0.73$
- $q \approx 0.9$
- $s(\varepsilon) \approx 1$



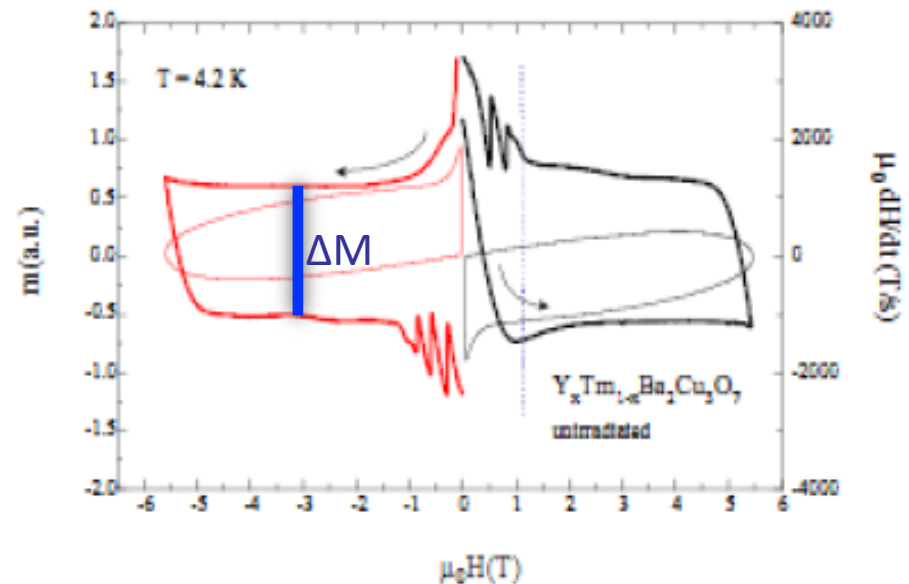
# Using magnetization data

- We have seen that the Meissner state corresponds to perfect diamagnetic behavior (type I superconductor)
  - We have seen that beyond  $H_{c1}$ , flux begins to penetrate and can be pinned at defects => hysteretic behavior; type II superconductor
- ⇒ *Much can be understood by measuring the effective magnetization of superconducting material*

**The measured magnetization provides insight into flux pinning and flux motion, key concepts governing the performance of superconducting materials.**

$$\Delta M \cdot B \propto F_p(T, B)$$

*Often used to evaluate  $J_c(B, T)$ !*

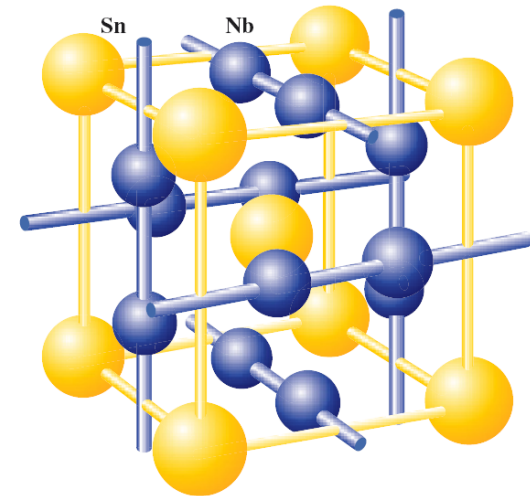
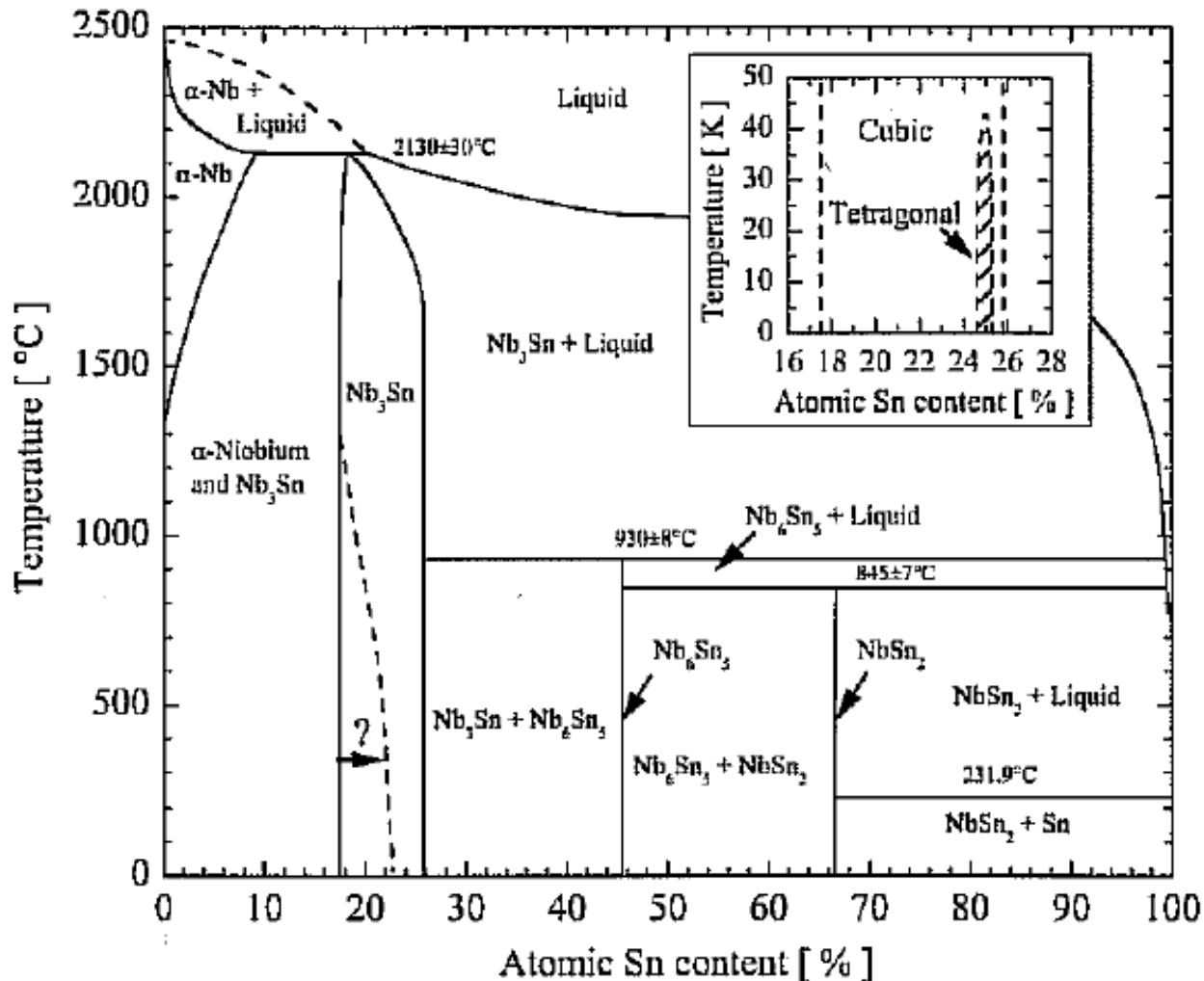


**J. Vanacken, et. al, 1999.**



# Example material: Nb<sub>3</sub>Sn

- Phase diagram, A15 lattice...





# Final comments

- Recent developments in  $T_c$  and  $J_c$  are quite impressive
  - Improvements in material processing has lead to
    - enhanced pinning
    - Enhanced  $T_c$
    - Smaller superconducting filaments
- Expect, *and participate in*, new and dramatic developments as fundamental understanding of superconductivity evolves and improvements in nanoscale fabrication processes are leveraged
  - A basic theory of superconductivity for HTS materials has yet to be formulated!
- Some understanding of the fundamentals of superconductivity are critical to appropriately select and apply these materials to accelerator magnets
  - Superconductors can be used to generate very high fields for state-of-the-art facilities, but they are *not* forgiving materials – *in accelerator applications they operate on a precarious balance of large stored energy and minute stability margin!*