

$$1) \quad TF = \frac{V}{R_{ref}} = \frac{G}{1+GH}$$

$$1.1) \quad GH \gg 1 \rightarrow \sim \frac{G}{1+GH} \approx \frac{G}{GH} = \frac{1}{H}$$

$$GH < 1 \sim G$$

$$1.2) \quad TF \approx G_0 + \Delta G \quad \text{when } GH \ll 1$$

we see the effect
in closed loop

$$TF \approx \frac{1}{H} \quad \text{when } GH \gg 1 \rightarrow \text{no effect due to disturbance}$$

$$1.3) \quad V = V_0 + \Delta V = (G_0 + \Delta G)(R_{ref} + \Delta R_{ref})$$

$$= \underbrace{G_0 R_{ref}}_{V_0} + G_0 \Delta R_{ref} + \Delta G R_{ref} + \Delta G \Delta R_{ref}$$

$$\frac{\Delta V}{V_0} \approx \frac{\Delta R_{ref}}{R_{ref}} + \frac{\Delta G}{G}$$

$$\left| \frac{\Delta V}{V_0} \right| < \left| \frac{\Delta R_{ref}}{R_{ref}} \right| + \left| \frac{\Delta G}{G} \right| \approx 0.1 \%$$

$$TF = \frac{KG}{1+KGH}, \quad KGH \gg 1 \Rightarrow \sim \frac{KG}{KGH} = \frac{1}{H}$$

~~$$\frac{V}{R_{ref}} = \frac{1}{H} \quad (V_0 + \Delta V) = \frac{R + \Delta R}{H + \Delta H}$$~~

~~$$H_0 \Delta V + H_0 V_0 + \Delta H \Delta V + \Delta H V_0 = R_{ref} + \Delta R$$~~

~~$$H \Delta V + \Delta H V_0 = \Delta R$$~~

~~$$\frac{\Delta V}{V_0} = \frac{\Delta R}{R_{ref}} + \frac{\Delta H}{H} \leq 2 \text{ppm}$$~~

2) ~~not~~

$$e = R_{ref} - HV$$

$$v = \frac{R_L}{R_L + R_0} A e = \frac{R_L}{R_L + R_0} A (R_{ref} - HV)$$

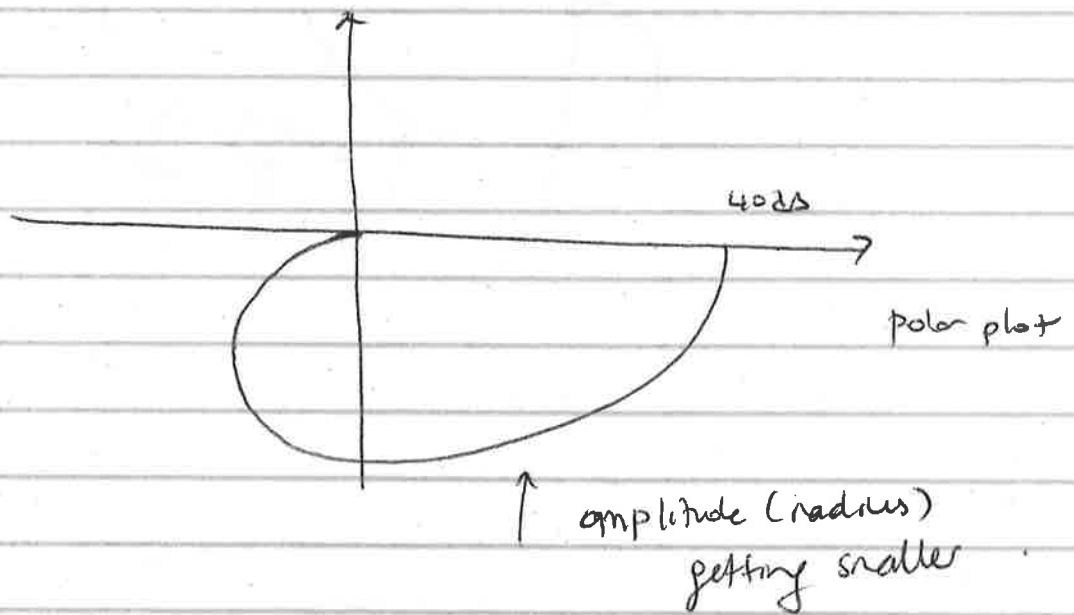
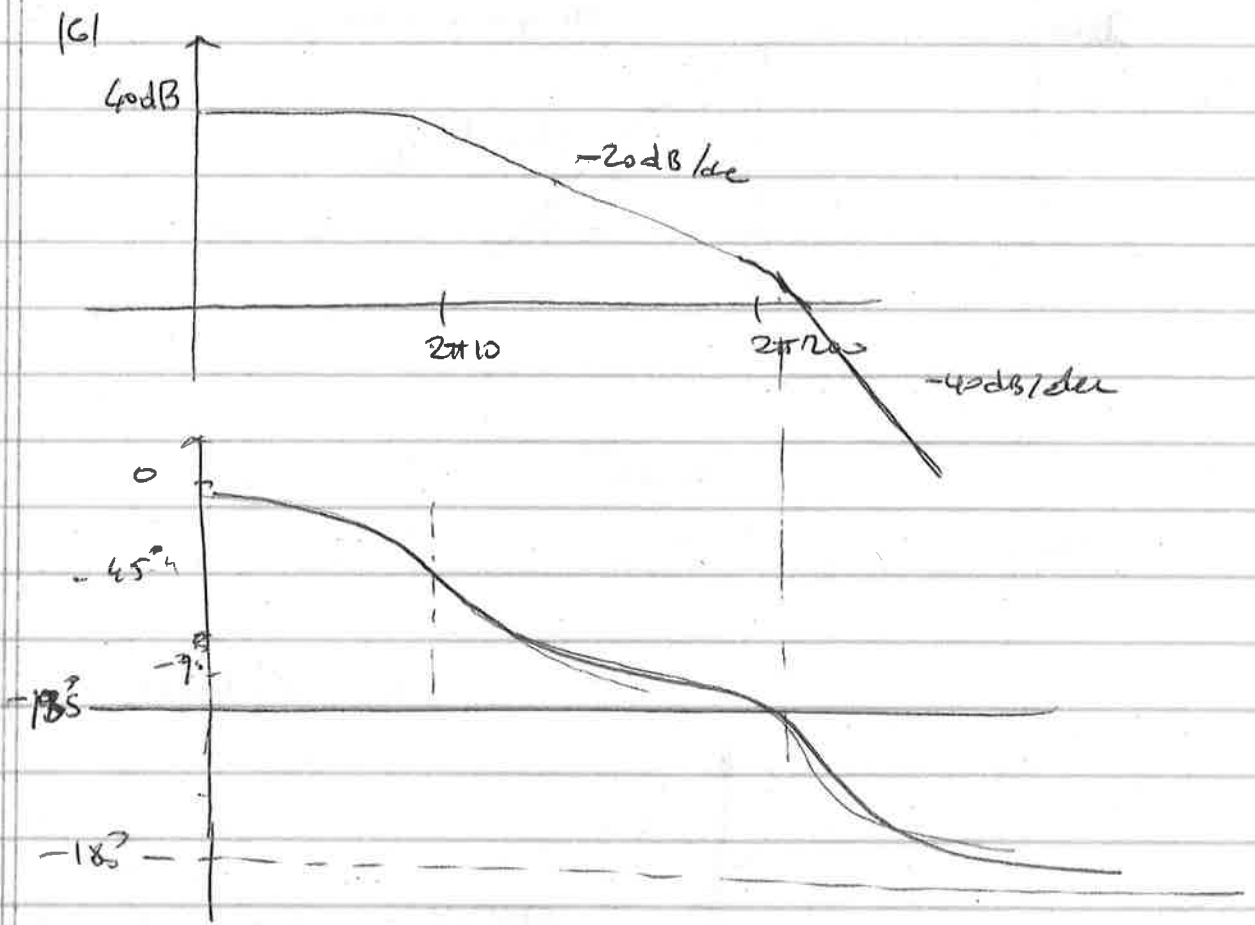
$$v \left(1 + \frac{R_L A H}{R_L + R_0} \right) = \frac{A R_L}{R_L + R_0} R_{ref}$$

$$\frac{v}{R_{ref}} = \frac{\frac{A R_L}{R_L + R_0}}{1 + \frac{R_L A H}{R_L + R_0}} = \frac{A R_L}{R_L + R_0 + R_L A H}$$

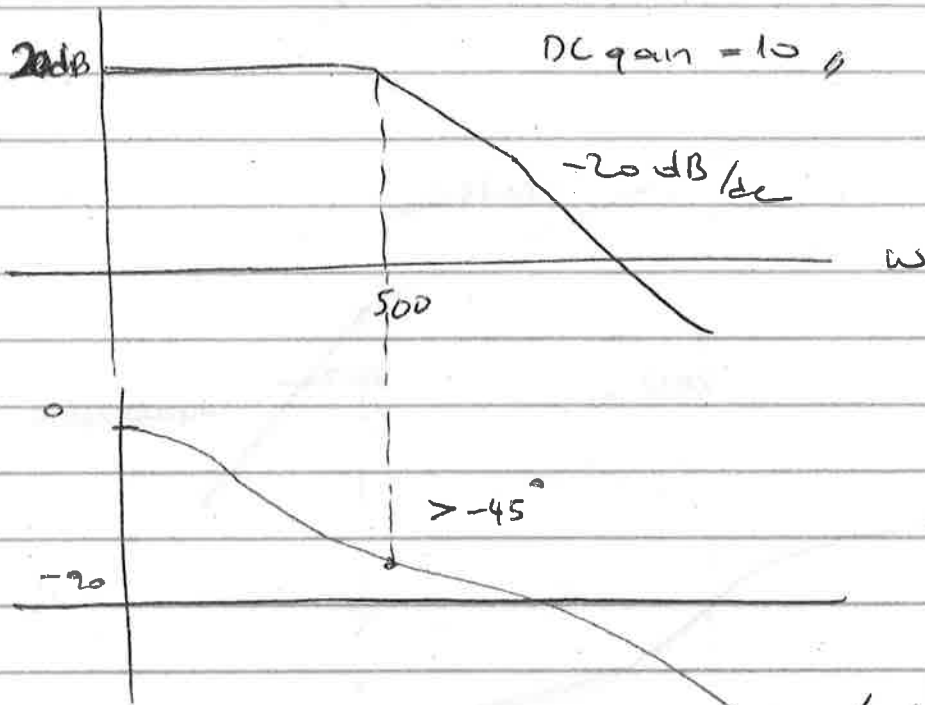
$$b) I_{out} = \frac{v - A e}{R_0} = \frac{v + A H v}{R_0} = \frac{v}{R_0} \frac{1 + A H}{1 + A H}$$

$$Z_{out} = \frac{v}{I_{out}} = \frac{R_0}{1 + A H} //$$

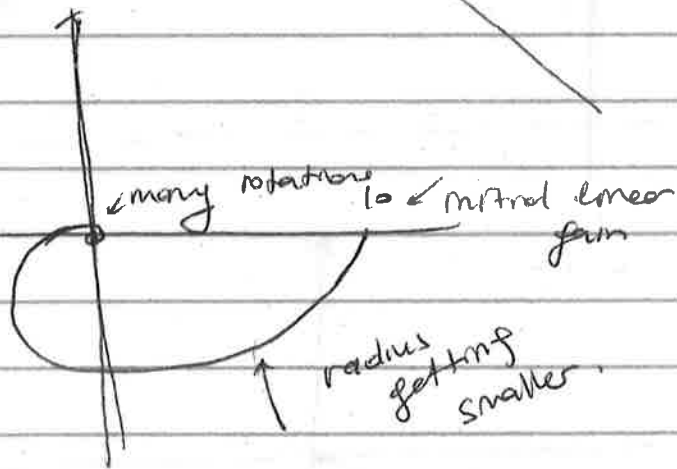
3) $G(s) = \frac{100}{(1 + s/2\pi 10)(1 + s^3/2\pi 200)}$



$$G(s) = \frac{5000 e^{-1ms}}{s + 500}$$



Effect of ~~phase~~ time delay



$$a) \frac{s+a}{(s^2 + 2\zeta\omega_0 s + \omega_0^2)(s+b)}$$

$$b < a \quad b < \zeta\omega_0 < a \quad \zeta < 1$$

$$s \quad \frac{-b \mp \sqrt{b^2 - 4ac}}{2a}$$

↖

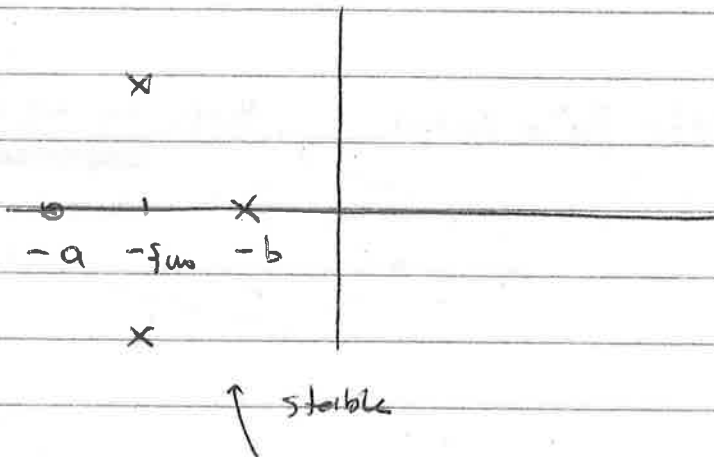
↗

$$(a s^2 + b s + c)$$

$$\frac{-2\zeta\omega_0 \mp \sqrt{4\zeta^2\omega_0^2 - 4\omega_0^2}}{2} = \frac{-\zeta\omega_0 \mp \sqrt{(\zeta^2 - 1)\omega_0^2}}{1}$$

$$= \frac{-\zeta\omega_0 \mp \omega_0 \sqrt{\zeta^2 - 1}}{1} \quad \zeta > 1$$

$$= -\zeta\omega_0 \mp j\omega_0 \sqrt{1 - \zeta^2}$$



$$b) \frac{s-a}{s^2 + bs + c} \rightarrow \text{Zero} = a$$

$$\text{poles} = \frac{-b \mp \sqrt{b^2 - 4ac}}{2a}$$

if $b^2 - 4ac < 0$ poles are $\frac{-b \mp j\sqrt{4ac - b^2}}{2a}$ ← complex

if $b > 0$ stable →

if $b^2 - 4ac > 0$ and $b > 0$ and $\frac{-b \mp \sqrt{b^2 - 4ac}}{2a}$

$\frac{-b + \sqrt{b^2 - 4ac}}{2a}$

$\frac{-b - \sqrt{b^2 - 4ac}}{2a}$

stability depends on b, c

↗ can be negative or positive

c)
$$\frac{s-a}{(s-a)(s+b)}$$

↓ this transfer function is stable

← pole zero cancellation

d)
$$\frac{k}{s^5 + 5s^3 + 4s^2 + s}$$

→ this is unstable, missing term

e)
$$\frac{k}{s^4 + 5s^3 - 3s^2 + 2s + 1}$$

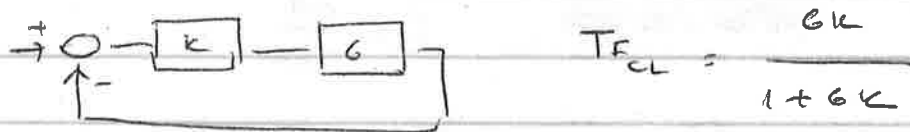
→ this is unstable
~~unstable~~
coefficient is (-)

Important note: In general pole-zero cancellations are really dangerous. Mathematically it looks like the system is stable but in reality pure pole-zero cancellations are very difficult so a system with pole-zero cancellation on an unstable pole is practically unstable!!

$$4) \quad G(s) = \frac{1360}{s+1360}$$

$$|G(s)|_{s=j\omega} = |G(s)|_{DC} \cdot \frac{1}{\sqrt{2}} \quad (-3dB)$$

$$|G(s)|_{j\omega} = \frac{\sqrt{1360^2}}{\sqrt{j\omega^2 + 1360^2}} = \frac{1}{\sqrt{2}} \rightarrow \omega_{pw} = 1360$$



$$TF_{CL} = \frac{GK}{1+GK}$$

$$K=10 \quad TF_{CL} = \frac{13600/s+1360}{1 + \frac{13600}{s+1360}} = \frac{13600}{s+1360+13600} = \frac{13600}{s+14960}$$

$$|G(s)|_{s=j\omega_{pw}} = |G(s)|_{DC} \cdot \frac{1}{\sqrt{2}} = \frac{13600}{14960} \cdot \frac{1}{\sqrt{2}}$$

$$\omega_{pw} = 14925 \approx$$

$$K=100 \quad TF_{CL} = \frac{136000}{s+137360} \quad \omega_{pw} \approx 137030 //$$

$$CL TF = \frac{GK}{1+GK} = \frac{\frac{1360K}{s+1360}}{1 + \frac{1360K}{s+1360}} = \frac{1360K}{s+(K+1)1360}$$

$$\Delta_{ch} = s + (K+1)1360 \rightarrow$$

$$\Delta_{ch} = 0 \Rightarrow s = -(K+1)1360 > 0 \quad \text{unstable}$$

$$K > -1 \rightarrow \text{stable}$$

$$T_{FCL} = \frac{6K}{1+6K} \cdot e^{-T_d s} \quad \text{where } T_d = 1 \times 10^{-6} \text{ s}$$

$$\Delta \theta_{\text{needed}} = -90^\circ$$

at what ω , $e^{-T_d s} = e^{-T_d j\omega} \Rightarrow$ will introduce 90 phase shift.

~~$$\frac{d\phi}{d\omega}$$~~

$$\tau = \frac{d\phi}{d\omega}$$

$$\Delta \phi = \omega (T_d) \Rightarrow \frac{\pi}{2} = (2\pi f) \cdot 1 \times 10^{-6} \text{ s}$$

\downarrow since this is constant $\downarrow \frac{1}{s}$

watch careful about units.

$$\omega = \frac{\pi}{2 \times 10^{-6}} = \frac{\pi}{2} \times 10^6 \text{ rad/s}$$

what is the gain of the system at this frequency, it shouldn't be 1.

$$|T_{FCL}|_{\omega = \frac{\pi}{2} \times 10^6} = \left| \frac{1360 \text{ Kertical}}{\Delta + 1360 + 1360 \text{ Kertical}} \right| = 1$$

$$\textcircled{2} j\omega$$

$$\omega = \frac{\pi}{2} \times 10^6$$

$$\frac{(1360 \text{ Kertical})^2}{\left(\left(\frac{\pi}{2} \times 10^6 \right)^2 + (1360 \text{ Kertical})^2 \right)} = 1$$

$$\left(j \frac{\pi}{2} \times 10^6 \right)^2 + \left((1360 \text{ Kertical})^2 \right)$$

$$\text{Kertical} \approx 1122 //$$

46.8dB

$$T_{F_{LL}} = \frac{136000}{k_{5700} s + 137360}$$

$$\frac{\sqrt{(136000)^2}}{\sqrt{j\omega^2 + 137600^2}} = 1$$

~~NA~~

$$\frac{136000^2}{\#} = (j\omega)^2 + (137600)^2$$

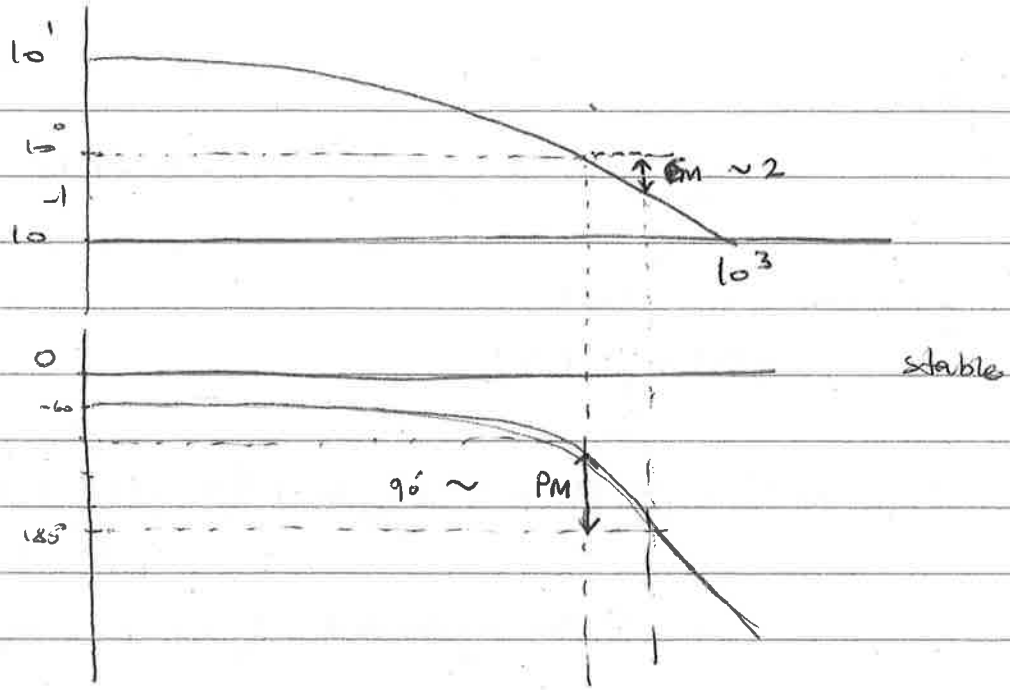
$$\omega = 19281 \text{ rad/s}$$

$$\theta = \omega \tau_{\text{Delay}}$$

$$\theta_{\text{max}} = 90^\circ$$

$$\frac{\theta_{\text{max}}}{\omega} = T_D \Rightarrow \frac{\pi/2}{19281} = 8.1467 e^{-5} \text{ seconds} = 0.81467 \mu\text{s}$$

5)



b) $\rightarrow GM \sim 2$

c) $3 > GM \rightarrow$ unstable

Problem 6)

$$\dot{\tilde{v}}_c(t) = (-\sigma - j\Delta\omega) \tilde{v}_c(t) + R_L \tilde{i}_T(t)$$

$$\tilde{v}_c(t) = v_{in}(t) + jv_\varphi(t)$$

$$\tilde{i}_T(t) = i_{in}(t) + ji_\varphi(t)$$

$$\begin{aligned} v_{in}(t) + j\dot{v}_\varphi(t) &= (-\sigma - j\Delta\omega) (v_{in}(t) + jv_\varphi(t)) \\ &\quad + R_L (i_{in}(t) + ji_\varphi(t)) \\ &= -\sigma v_{in} - j\Delta\omega v_{in} - \sigma jv_\varphi + \Delta\omega v_\varphi + R_L i_{in}(t) + R_L j i_\varphi \end{aligned}$$

$$\dot{v}_{in} = -\sigma v_{in} + \Delta\omega v_\varphi + R_L i_{in}$$

$$j\dot{v}_\varphi(t) = -j\Delta\omega v_{in} - \sigma jv_\varphi + R_L j i_\varphi$$

$$\begin{bmatrix} \dot{v}_{in} \\ \dot{v}_\varphi \end{bmatrix} = \begin{bmatrix} -\sigma & \Delta\omega \\ -\Delta\omega & -\sigma \end{bmatrix} \begin{bmatrix} v_{in} \\ v_\varphi \end{bmatrix} + R_L \begin{bmatrix} i_{in} \\ i_\varphi \end{bmatrix}$$

MONDAY

$$\begin{aligned} 7) \quad Z_{co}(w) &= \frac{R_0}{1 + jR_0(wC - \frac{1}{wL})} = \text{then } Z_c(w) = Z_{co}(w) \parallel Z_{oo}(w) \\ &= \frac{R_0}{1 + jR_0(wC - \frac{1}{wL})} * N^2 Z_0 \\ &= \frac{N^2 Z_0 R_0}{N^2 Z_0 + \frac{R_0}{1 + jR_0(wC - \frac{1}{wL})}} = \frac{N^2 Z_0 R_0}{R_0 + N^2 Z_0 + jN^2 Z_0 R_0 (wC - \frac{1}{wL})} \\ &= \frac{N^2 Z_0 R_0}{N^2 Z_0 [1 + \beta + jR_0 (wC - \frac{1}{wL})]} = \frac{R_0 / (1 + \beta)}{1 + j \frac{R_0}{1 + \beta} (wC - \frac{1}{wL})} \\ &= \frac{R}{1 + jR (wC - \frac{1}{wL})} \end{aligned}$$

$$2) \quad Q_L = \frac{Q_0}{1 + \beta} = \frac{32 \times 10^3}{1 + 3.6} = \underline{6956}$$

$$R_L = \left(\frac{\Gamma}{Q} \right) \frac{1}{2} \cdot Q_L = \frac{233.1 \Omega}{2} \cdot 6956 = \underline{8.1 \times 10^5 \Omega}$$

$$3) \quad w_{1/2} = \frac{w_0}{2Q_L} = \frac{476 \times 10^6 \times 2 \times \pi}{2 \times 6956} = 2.15 \times 10^5$$

$$w_{1/2} = \frac{w_0}{2Q_0} = \frac{476 \times 10^6 \times 2 \times \pi}{2 \times 32 \times 10^3} = 4.67 \times 10^4$$

WEDNESDAY #1

$$P_g = \frac{\hat{V}_c^2}{4 \left(\frac{L}{Q}\right) Q_L} \left[\left(1 + \frac{\left(\frac{L}{Q}\right) Q_L I_{B0}}{\hat{V}_c} \cos \phi_b\right)^2 + \left(2 Q_L \frac{\Delta \omega}{\omega} + \frac{\left(\frac{L}{Q}\right) Q_L I_{B0}}{\hat{V}_c} \sin \phi_b\right)^2 \right]$$

a) $\hat{V}_c = 16 \text{ MV}$ $\Delta \omega = 0$, $I_{B0} = 0$

$$P_g|_c = \frac{(16 \text{ e}^6)^2}{4 (1036) 4.12 \times 10^7} = 1500 \text{ W} \quad \frac{1500}{0.9} = 1.67 \text{ kW}$$

$$P_g = P_{LWS} + P_g|_c = 1.1 P_g|_c = \underline{1650 \text{ W}}$$

b) $\frac{\left(\frac{L}{Q}\right) Q_L I_{B0}}{\hat{V}_c} = \frac{1036 \times 4.12 \times 10^7 \cdot 100 \text{ e}^{-6} \text{ A}}{16 \text{ e}^6 \text{ V}} = 0.2668$

$$P_g|_c = \frac{1500 \text{ W}}{\text{Part a)}} \left[(1 + 0.2668 \cos 30^\circ)^2 + (0.2668 \sin 30^\circ)^2 \right] = 2300 \text{ W}$$

$$P_g = 1.1 \times 2300 \text{ W} = \underline{2530 \text{ W}}$$

c) $2 Q_L \frac{\Delta \omega}{\omega} = \frac{2 \cdot 4.12 \times 10^7 \cdot 20^\circ}{2\pi \cdot 1.36 \text{ Hz}} = \frac{2 \cdot 4.12 \times 10^7}{2\pi \cdot 1.3 \text{ e}^9 \text{ Hz}} \cdot \frac{20^\circ}{180} = 1.2831$

$$P_g|_c = 1500 \text{ W} \left[(1 + 0.2668)^2 + (1.2831)^2 \right] = 4877 \text{ W}$$

at $\Delta \omega = \pm 20 \text{ Hz}$

$$P_g = 1.1 \times 4877 \text{ W} = \underline{5.364 \text{ kW}}$$