

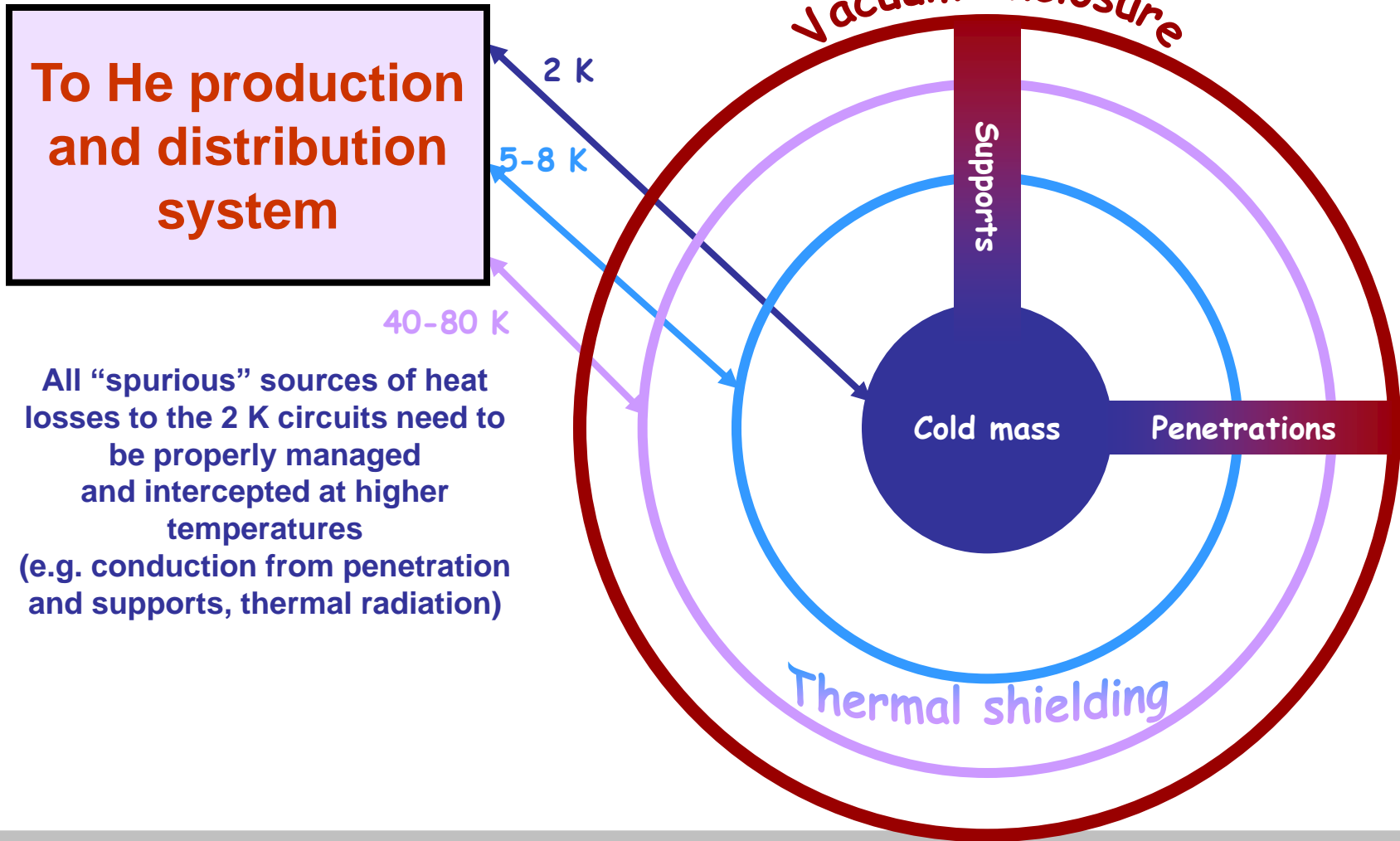
# CRYOSTATS

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Old Dominion University  
and**

**Thomas Jefferson National Accelerator Facility**

# “Cartoon” view of the system



# Basic Functions of a Cryomodule

- In SRF application the cryomodule provides:
  - **Cryogenic environment** for the cold mass operation
    - Cavities/Magnets in their vessels filled with sub atmospheric He at 2 K
    - He coolant distribution at required temperatures
    - Low losses penetrations for RF, cryogenics and instrumentation
  - **Shield for the sources of “parasitical” heat transfer** from room to cryogenics temperature produced by three mechanisms
    - thermal radiation
    - conduction
    - convection
    - (To mitigate loads at 2 K all heat fluxes need to be intercepted at higher T)
  - **Structural support** of the cold mass
    - Issues concerning different thermal contractions of materials
    - Provide precise alignment capabilities and reproducibility with thermal cycling
- The cryomodule contains a variety of complex technological objects: cavities and their ancillaries, but also magnets and BPMs

# Heat losses issues: Physical mechanisms

- Thermal radiation

$$\dot{Q} = S \varepsilon \sigma_{SB} (T_h^4 - T_c^4)$$

- Radiated power from hot surfaces to vanishingly temperatures is proportional to  $T^4$  (Stephan-Boltzmann).  $\sigma_{SB} = 5,67 \cdot 10^{-8} [\text{W m}^{-2} \text{K}^{-4}]$ 
  - Reduce the surface emissivity,  $\varepsilon$  (material and geometry issue)
  - Intercept thermal radiation at intermediate temperatures by means of thermal shields

- Heat conduction

- A SRF module has many penetration from the room temperature environment (RF couplers, cables, ...)
  - Proper choice of low thermal conduction,  $k_{th}$ , materials whenever possible
  - Minimize thermal paths from r.t. and provide thermalization at intermediate temperatures.

$$\dot{Q} = \frac{S}{L} \int_{T_c}^{T_h} k_{th}(T) dT$$

- Convection

- Convective exchange from r.t. is managed by providing insulation vacuum between the room temperature vessel and the cold mass

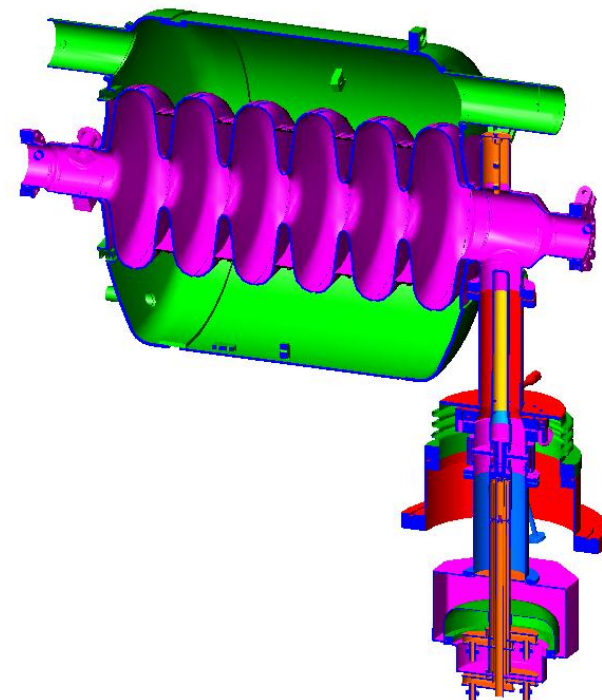
$$\dot{Q} = S h (T_h - T_c)$$

# Magnetic Shielding

- Reduce 1 G background field to  $< 10$  mG
  - Attenuation factor =  $1 / 0.010 = 100$ 
    - The 1 G background field includes earth's field as well as fields from other sources (ie. rebar and magnet stray fields)
- Minimize shielding cost
  - Maximize shielding performance
  - As much commonality between Medium and High Beta shields as possible
- Shield around components of cryomodule (geometric constraints)

# Instrumentation

Signal Description	Device	# Pins/ Device	Qty.	Feed-thru
RF	HOM	N/A	2	N-type
RF	Field Probe	N/A	1	N-type
Low I, V	Diode	2	4 (x2)	Part of 24-pin UHV Ceramic
Low I, V	Liquid Level	4	1*	Part of 24-pin UHV Ceramic
High I, V	Tuner Motor	2	1	Part of 24-pin UHV Ceramic
High I, V	Limit Switches	4	2	Part of 24-pin UHV Ceramic
High I, V	Heater	4	1	Part of 24-pin UHV Ceramic
Vacuum	Cold Cathode Gauge	N/A	1 (x2)	SHV
Vacuum	Thermocouple Gauge	N/A	1	Standard TC Gauge Connector



# Instrumentation (SNS CM)

- Liquid Helium Level Sensor
  - CEBAF Drawing # 11161-C-0069 (American Magnetics, Inc.)
  - Quantity : 2 per CM, located in Helium Vessels nearest each End Can
  - Supported from Cavity Reinforcing Ring
  - Modifications for Radiation Resistance:
    - Kapton Leads
    - Replace Teflon Plug
  - Other Modifications:
    - Additional Sheath required to stabilize readings
- Pressure Transducer
  - Baratron, Range: 0-100 Torr
  - Quantity : 1 per CM
  - Located on Return End Can to measure return pressure PRIOR to HX
  - Accessible in Tunnel therefore redundant sensors not required.

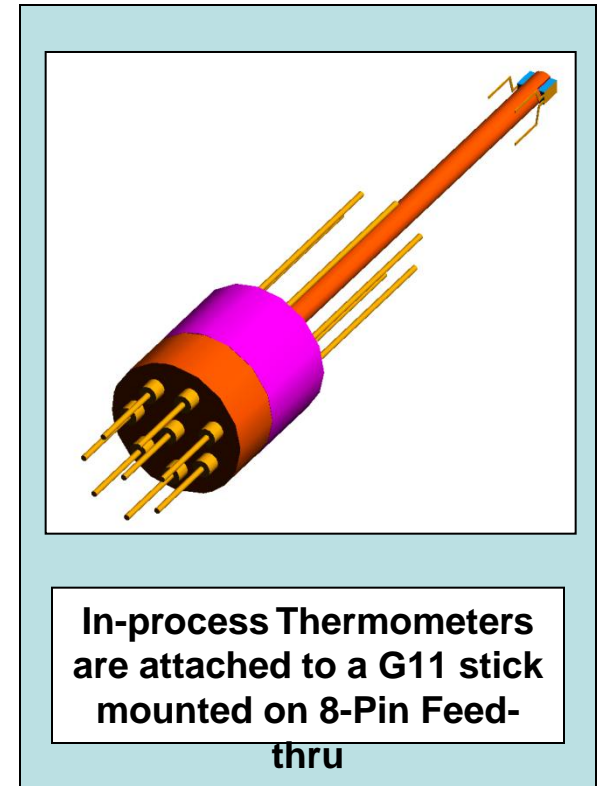
# Instrumentation (SNS CM)

- Heaters
  - Minco P/N HK15097, 100 W, 28 Vdc, 7.8  $\Omega$  (Used in Original CEBAF)
  - Quantity : 1 per Helium Vessel
  - Mounting:
    - Heater is attached to G11 card with acrylic adhesive
    - Card is bolted to block inside HV shell
  - Modifications for Radiation Resistance:
    - Kapton Leads
    - G11 Substrate
    - Acrylic Adhesive



# Instrumentation (SNS CM)

- Thermometry
  - Measurements:
    - Cavity cell and beam pipe temperatures
    - Primary and shield process temperatures
    - Heat Exchanger Terminal Temperatures
    - FPC Outer Conductor and Water Temps
  - Outside CM: Thermocouples (FPC Warm End)
    - Less expensive than RTDs or Diodes
    - Simplifies control system
  - Inside CM: Cernox CX-1050-SD OR DT-470-SD
    - Both are 4-wire hermetic chip packages
    - Quantities per CM :
      - Medium  $\beta$  – 20(x2 per location)
      - High  $\beta$  – 24(x2 per location)
    - Mounting: Chip is epoxied in place, leads are heat sunk



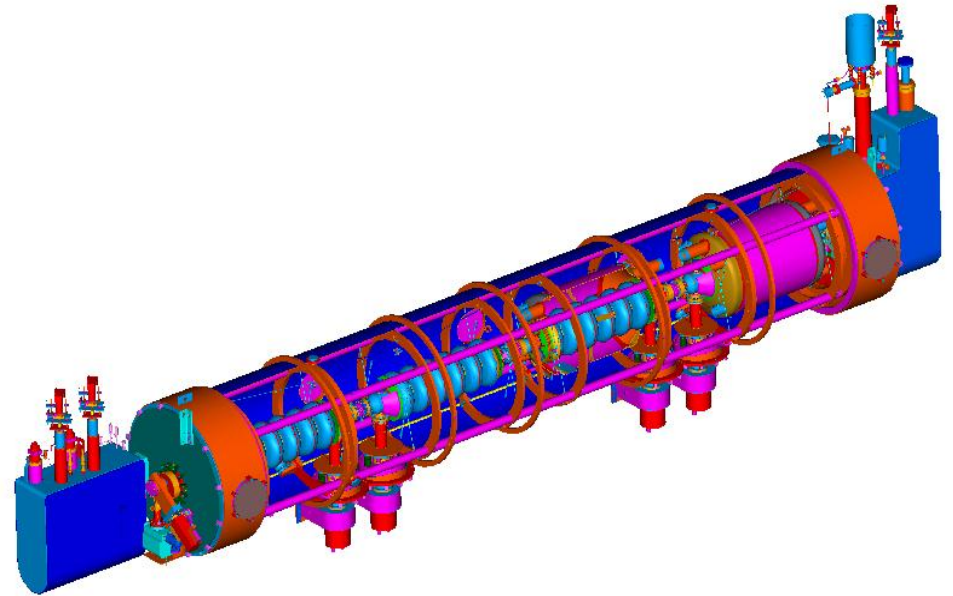
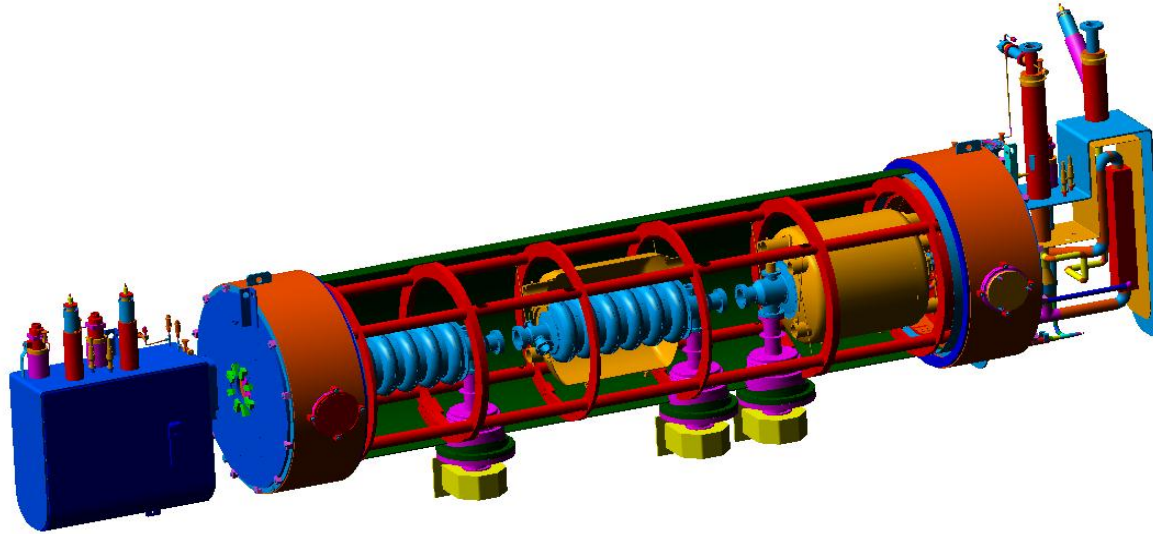
# Cernox vs. Silicon Diodes

- Technical:
  - Cernox has higher radiation resistance
  - Silicon Diodes can be recalibrated in-situ using a pressure measurement with Baratron Gauge
  - Control system more complex for Cernox approach
- Cost: Cernox is more expensive (~250K)
  - Calibrated Cernox RTDs are 2 times more expensive than grouped Diodes (\$537 vs \$385) - ~\$150 K
  - More complex controls for Cernox costs ~\$100K (per H. Strong Estimate)

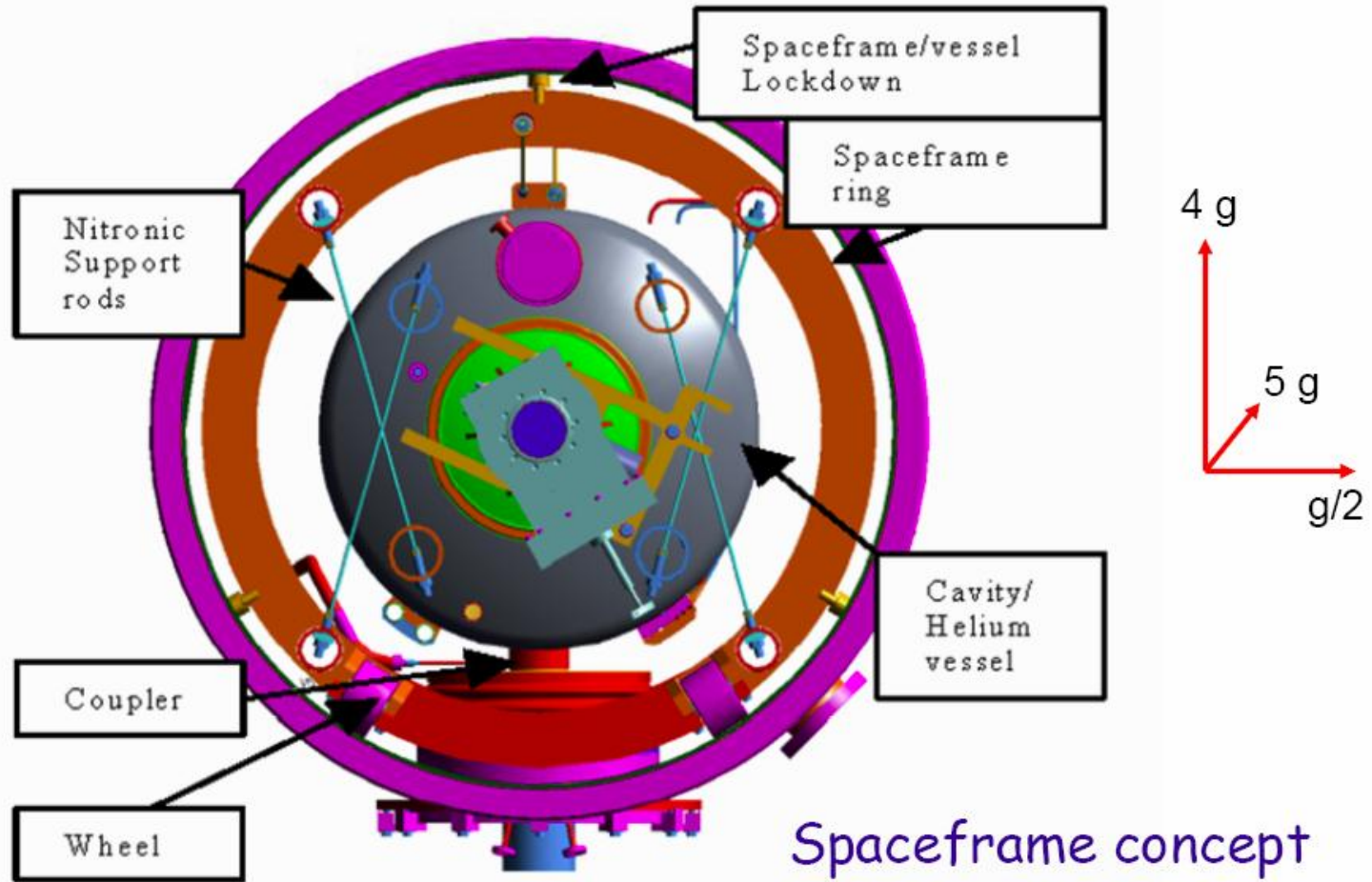
# FPC Instrumentation

- Infrared Sensor
  - 1 per FPC
  - Monitors window temperature
- Arc Detector
  - 1 per FPC
  - Custom Photo-multiplier Tube Design
- Cold Cathode Gauge
  - 1 per FPC; sense pressure spikes during operation
  - Balzers, coaxial design, P/N IKR 060
- RTD/Diode on Outer Conductor (See Cavity Instrument Listing)
- Thermocouples near Warm End
  - 3 per FPC ; Water inlet & outlet, Helium Exhaust Temperature; K-Type
- Window Heater
  - 1 per FPC; mounted on Window-to-Outer-Conductor Flange
  - 100 W, 28 Vdc, 7.8  $\Omega$
- Voltage Bias

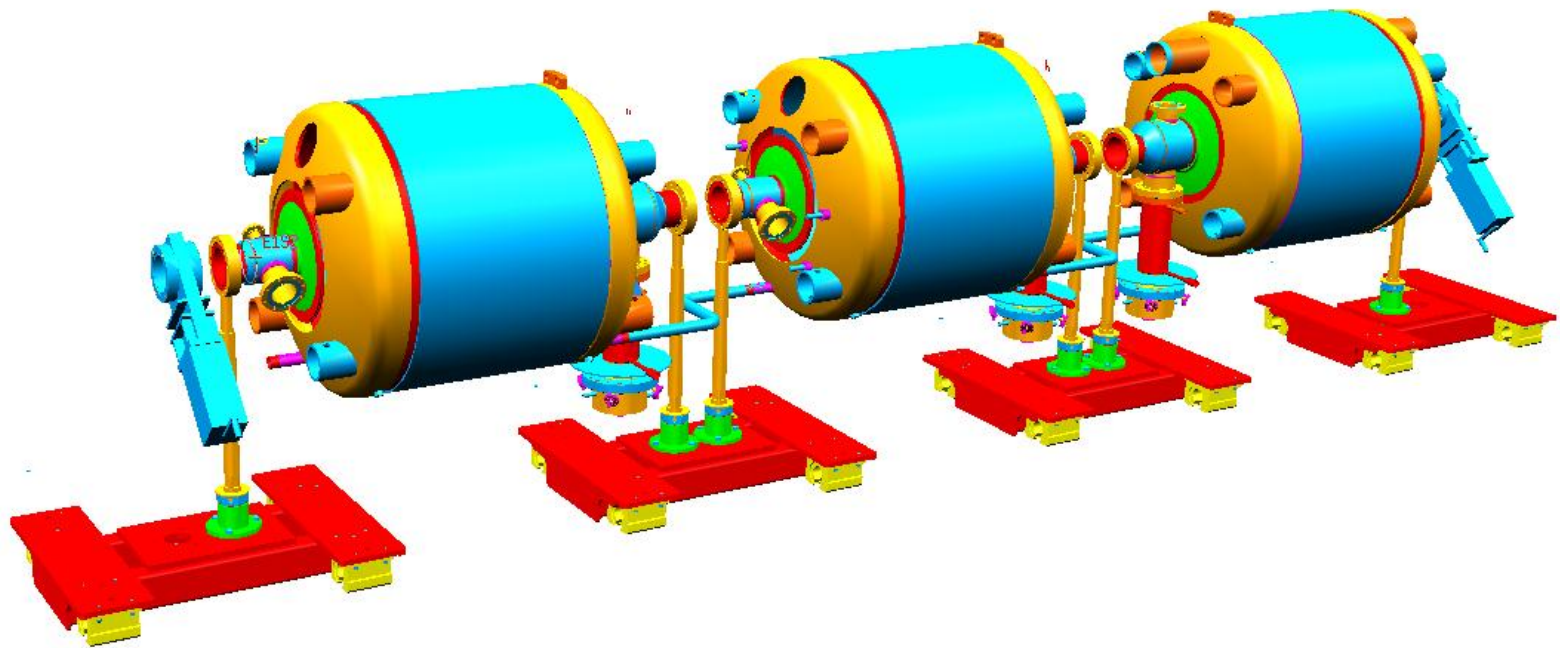
# SNS Medium and High Beta Cryomodules



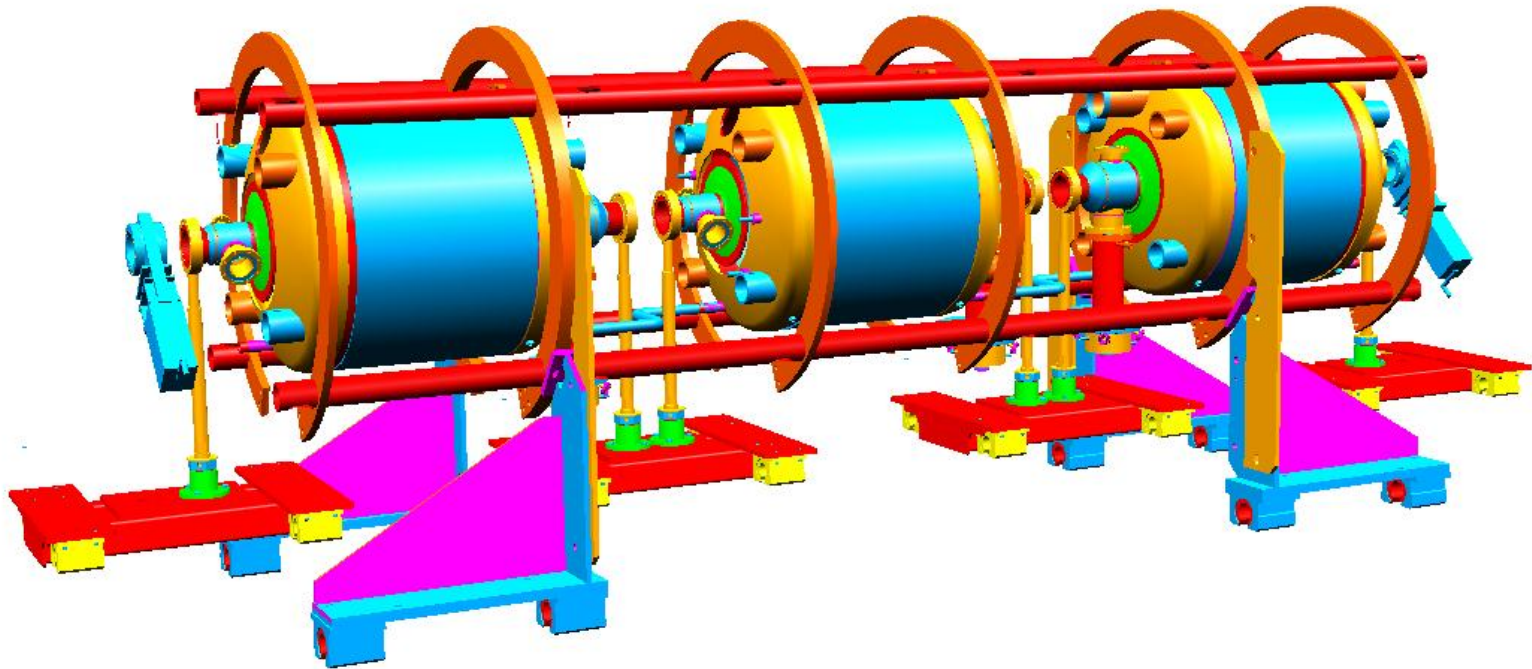
# Cross Section



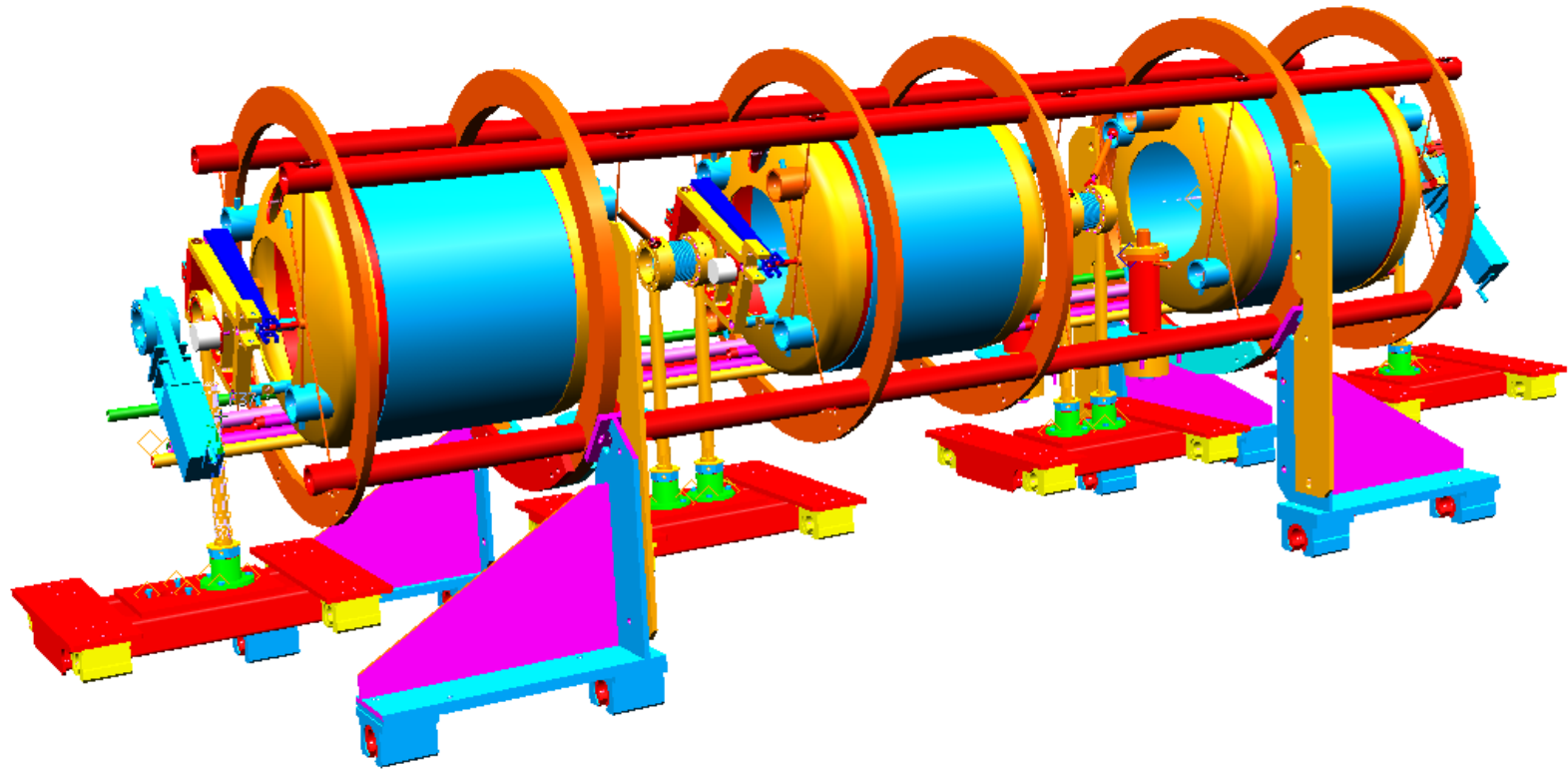
# Cavity String Assembly on Cavity Assembly Bench in Clean Room



# Installation of Frame Over Cavity String on CM Assembly Bench

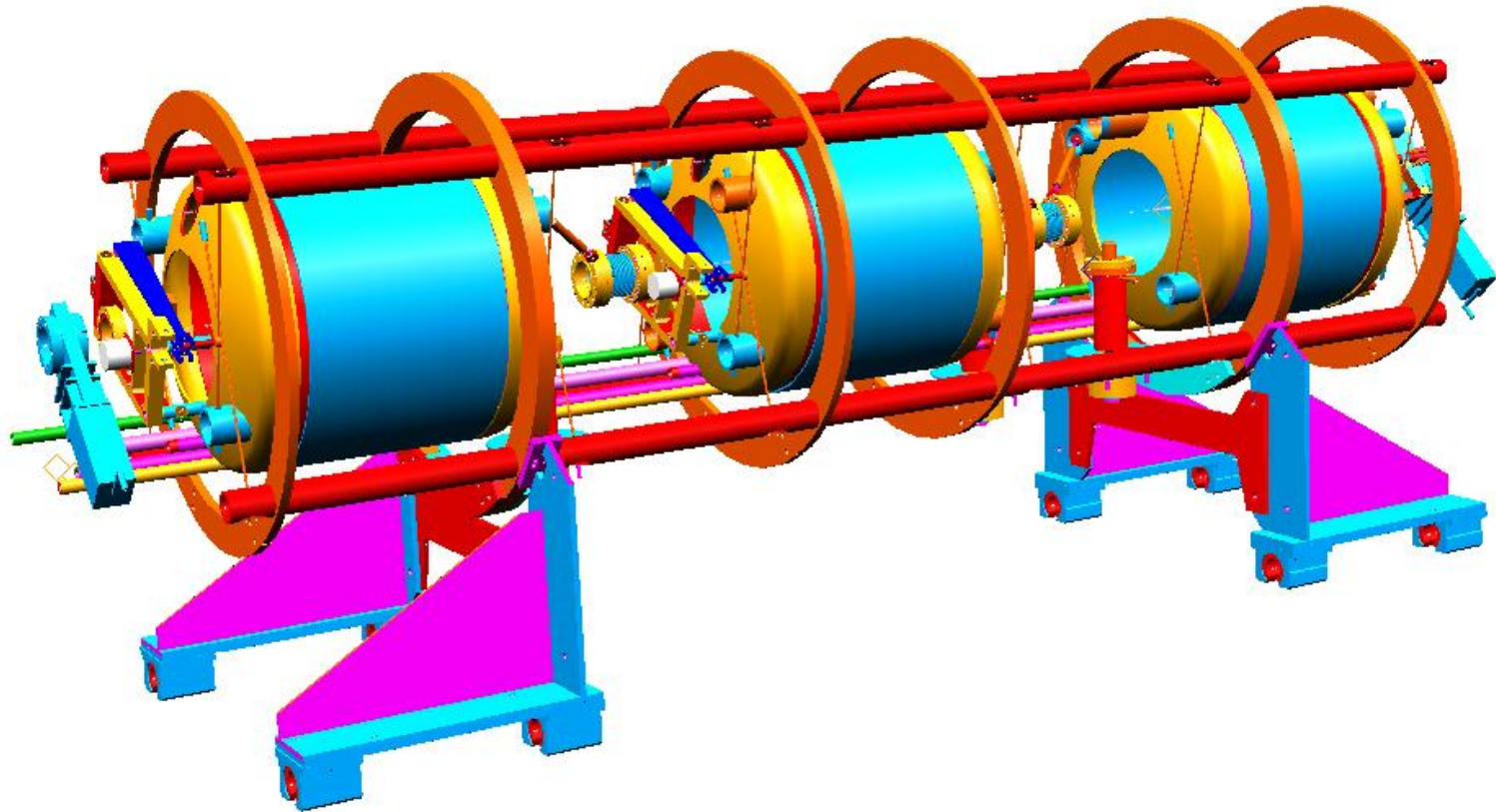


# Cavity String Support Transfer from Lolly Pops to Nitronic Rods

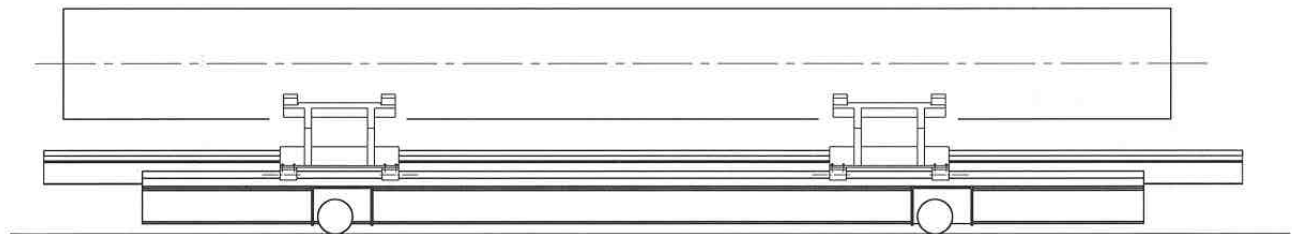
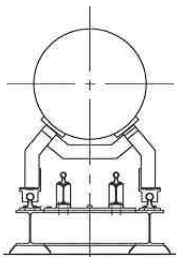




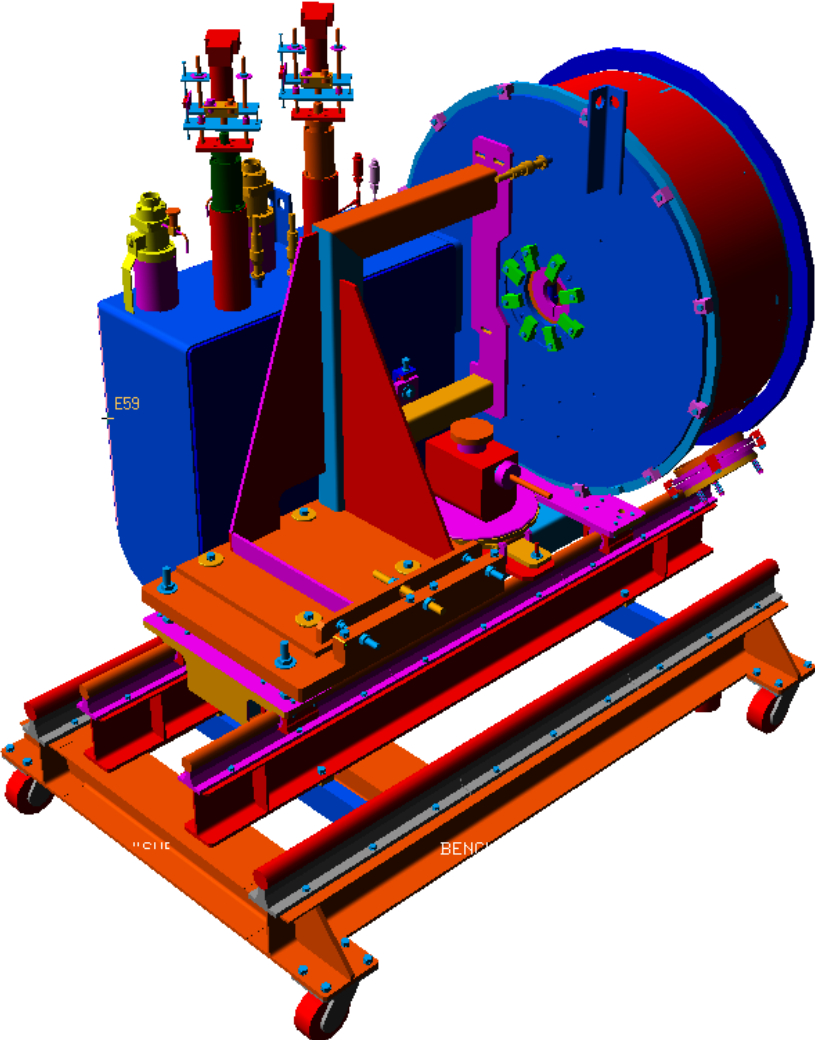
# String Supported on Space Frame, To Be Inserted In Vacuum Tank



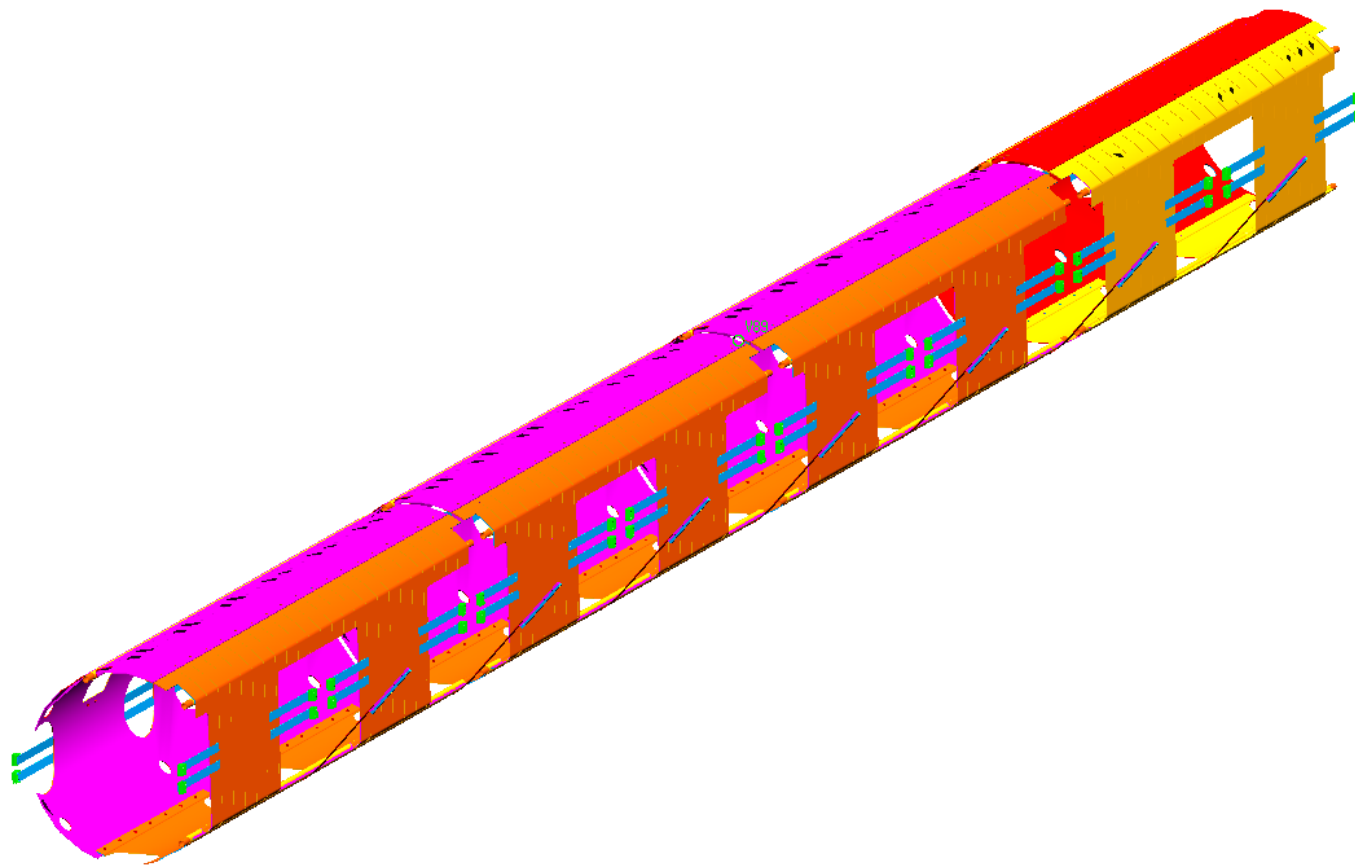
# Transfer Bench with Vacuum Tank Ready to Accept Space Frame



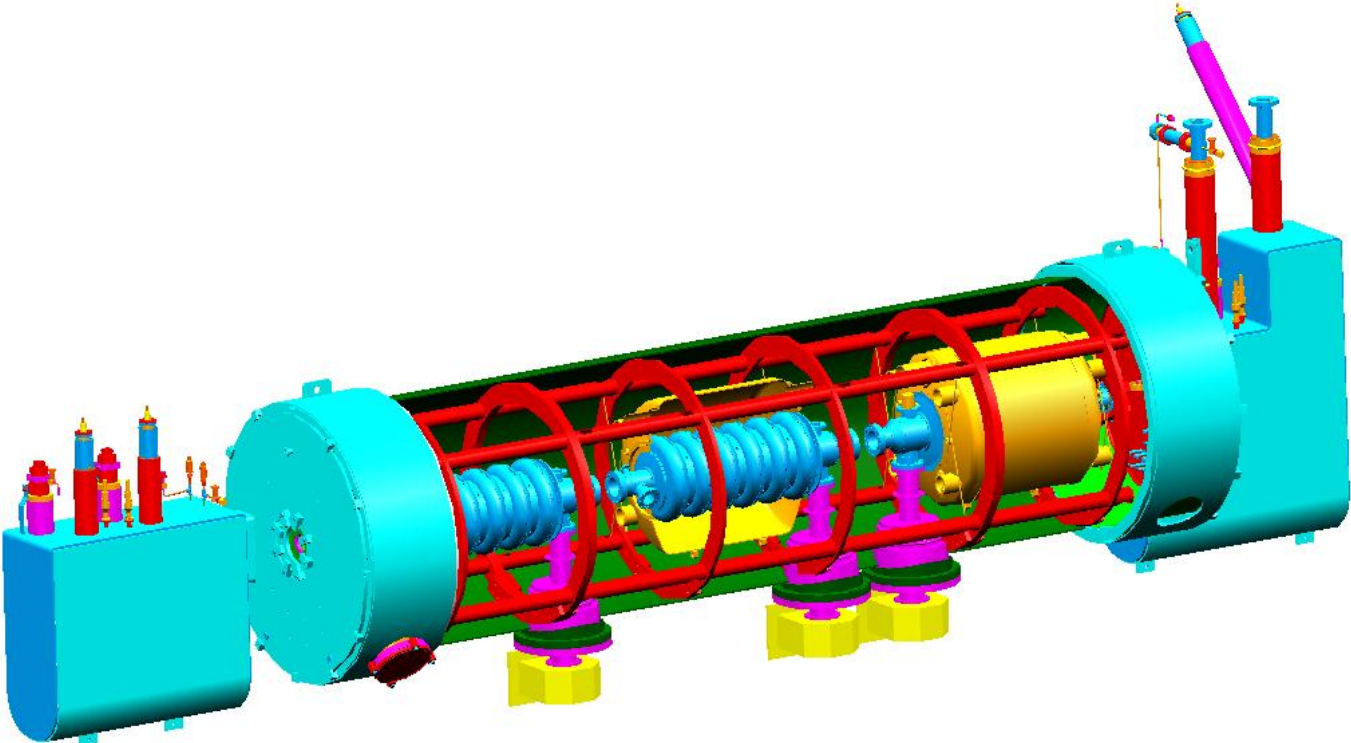
# Installation of End Can on to Assembly Bench



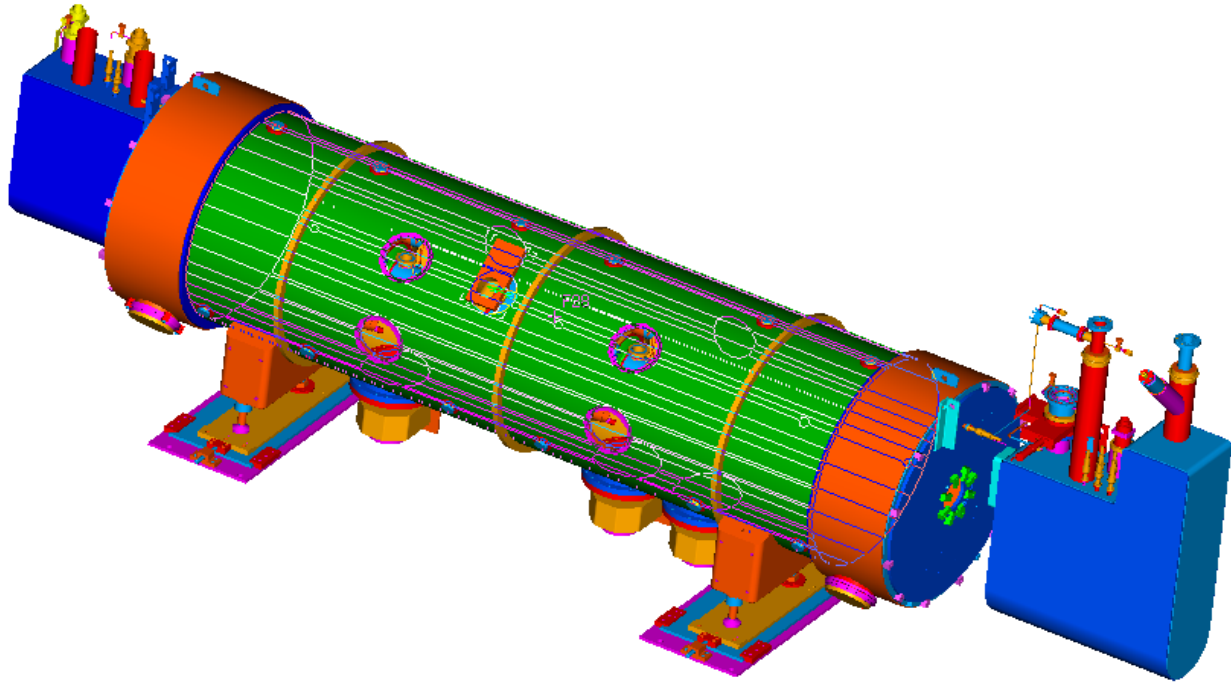
# Shield Assembly (Upgrade)



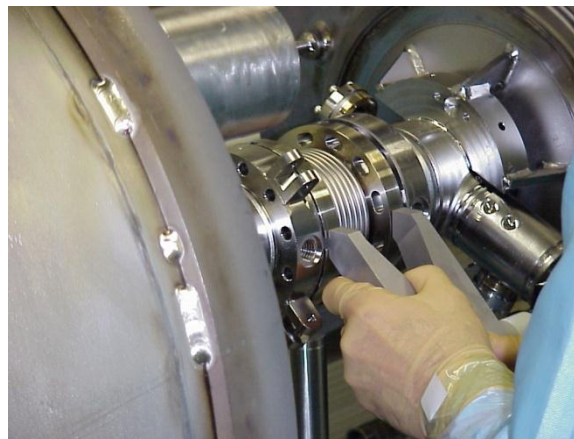
# Production Cryomodule Cut-a-way

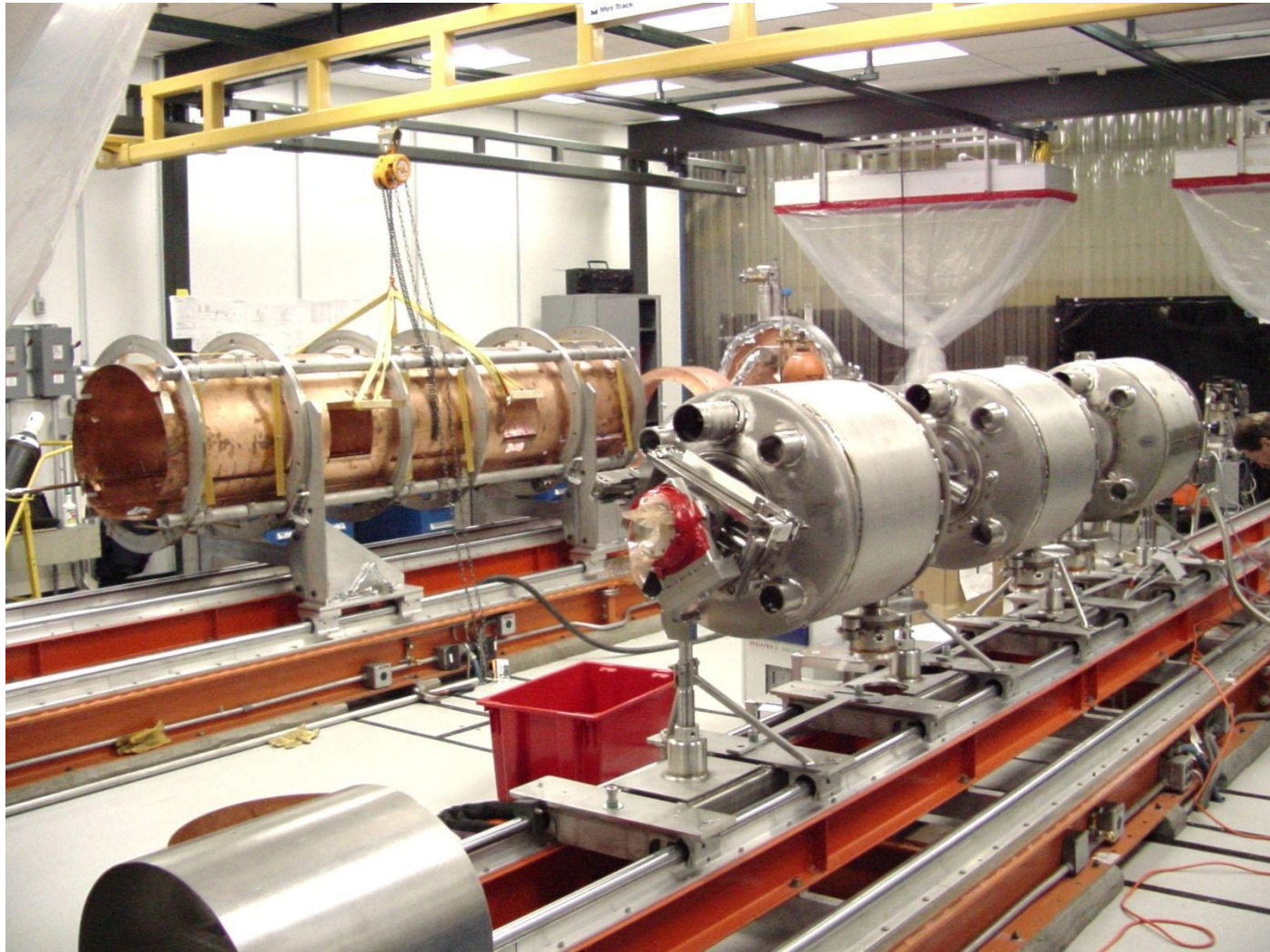


# Completed Cryomodule on Support Stands

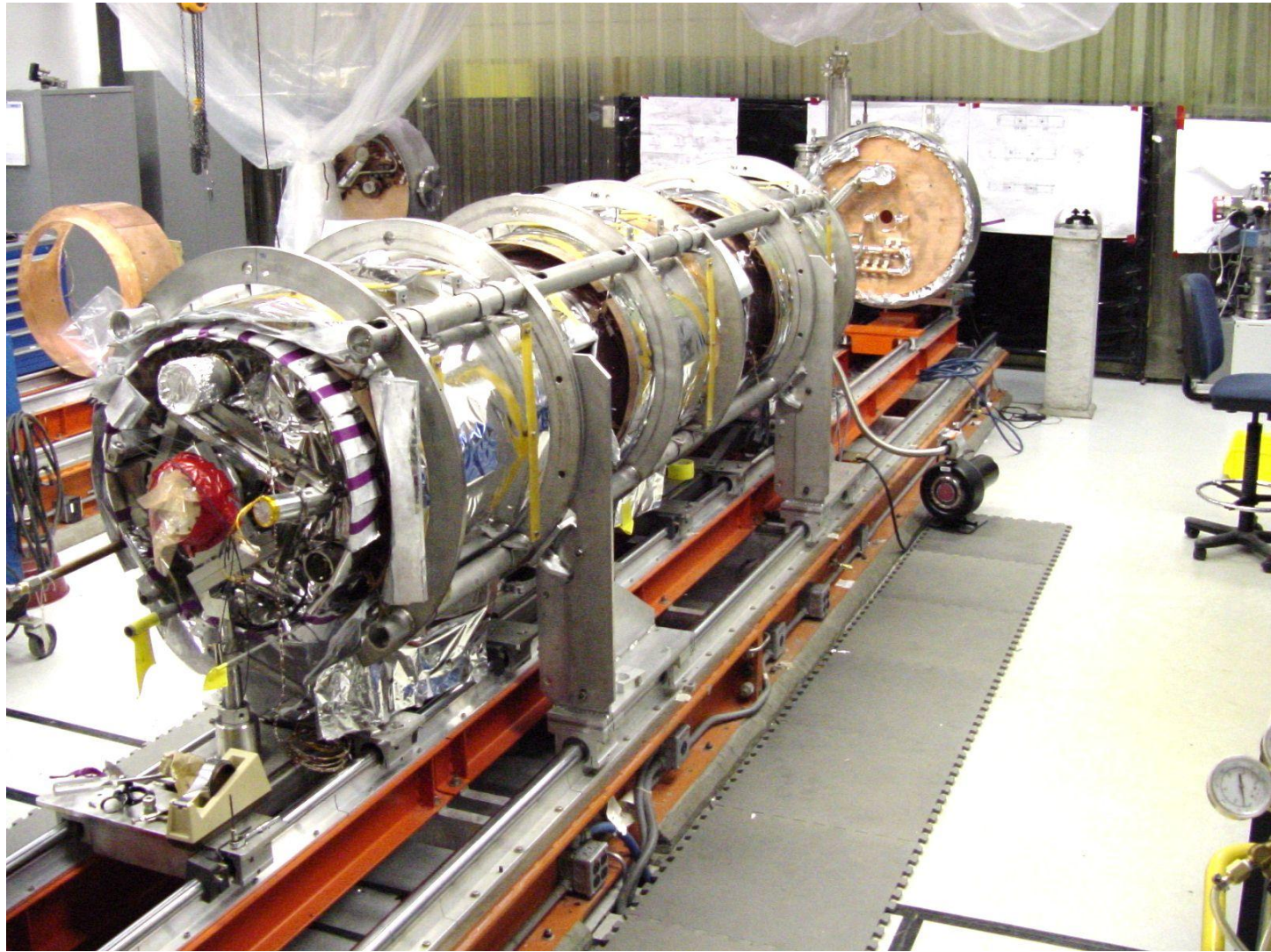


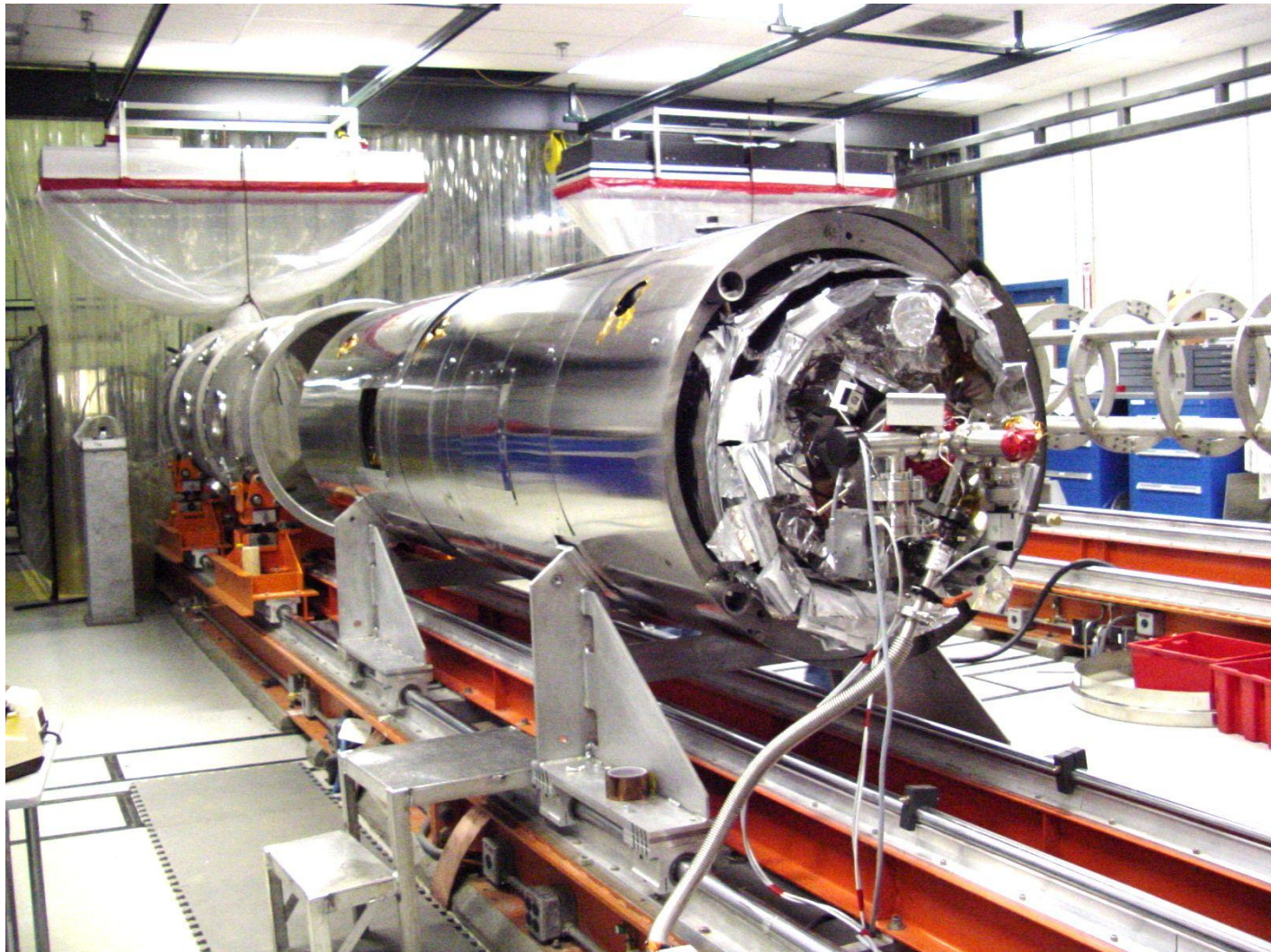
# Cavity String Assembly



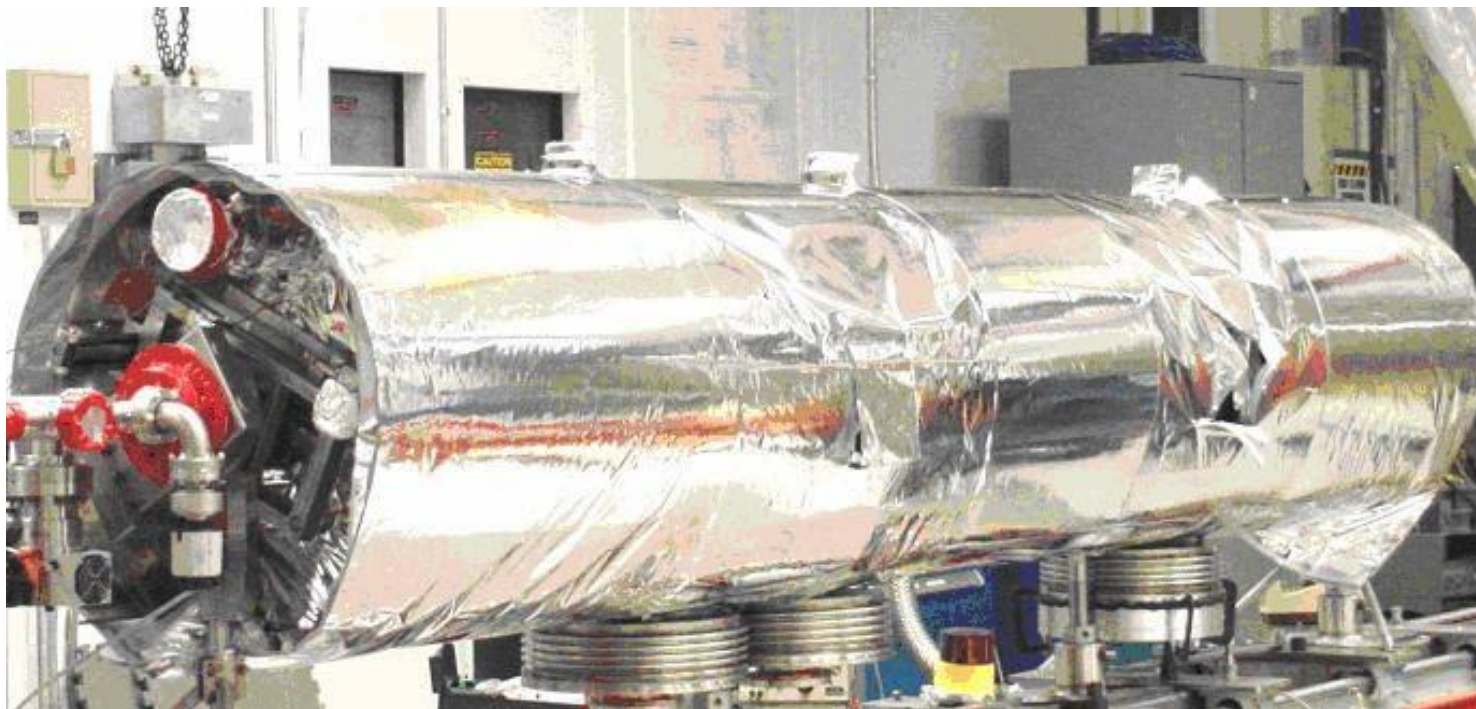


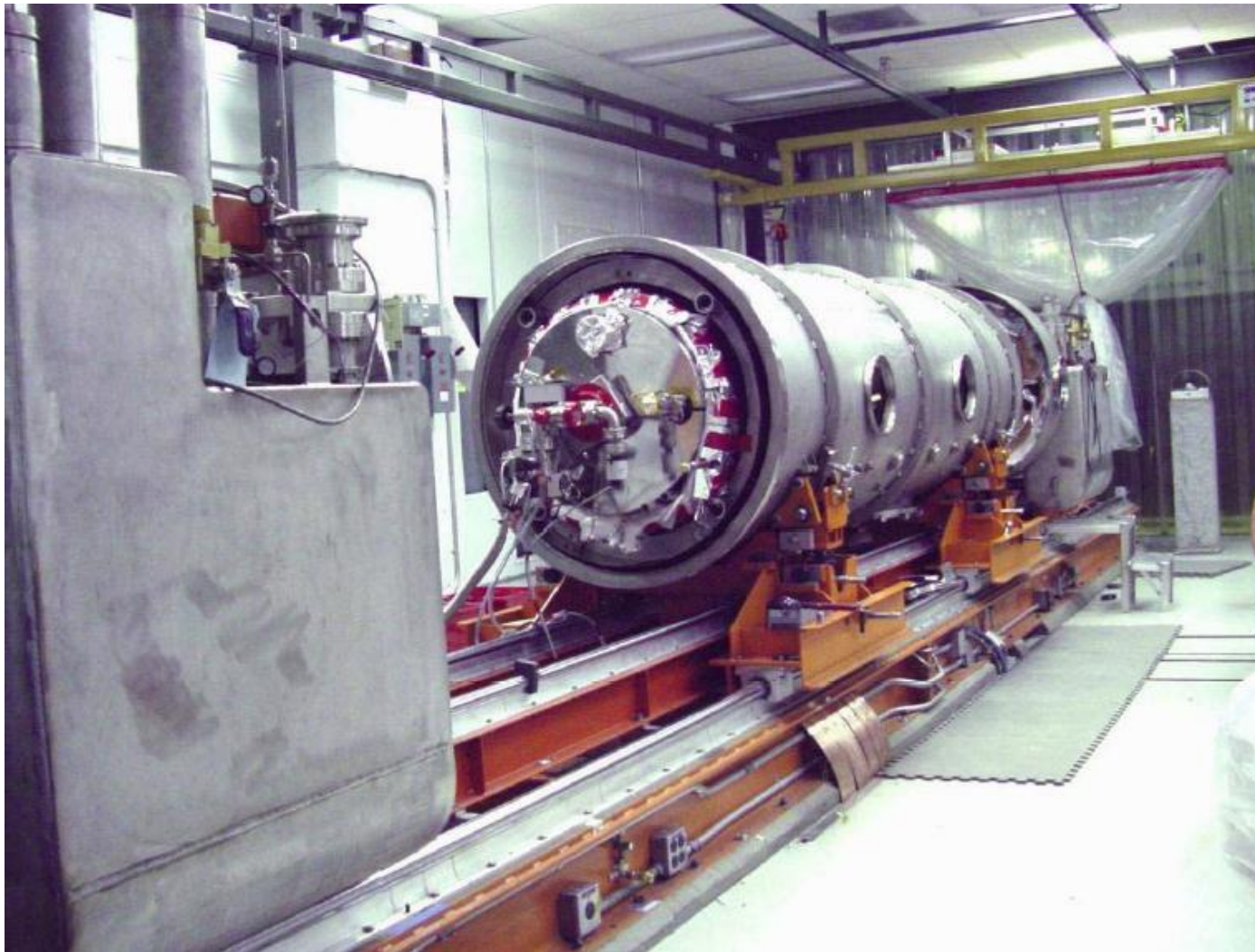




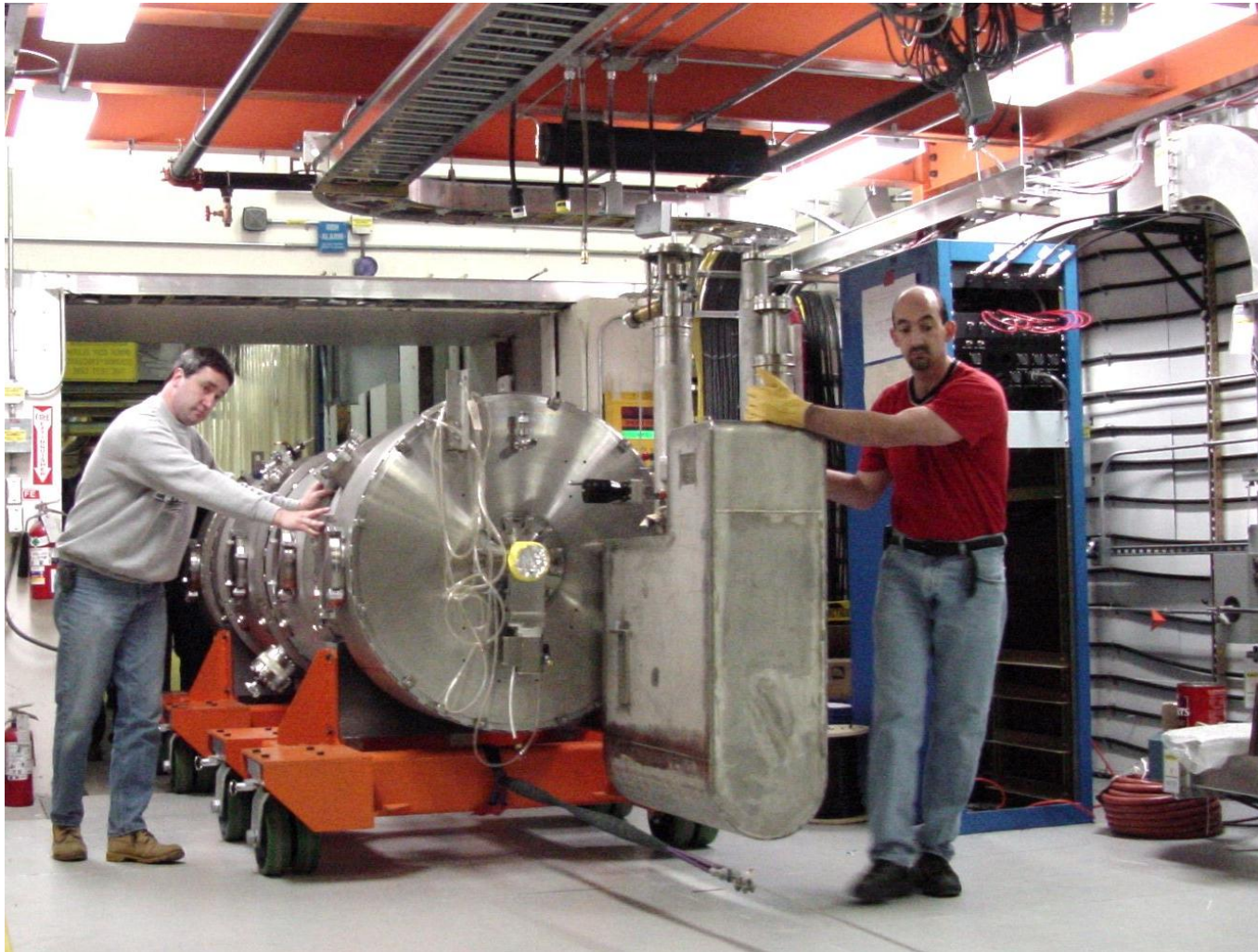


# Superinsulation





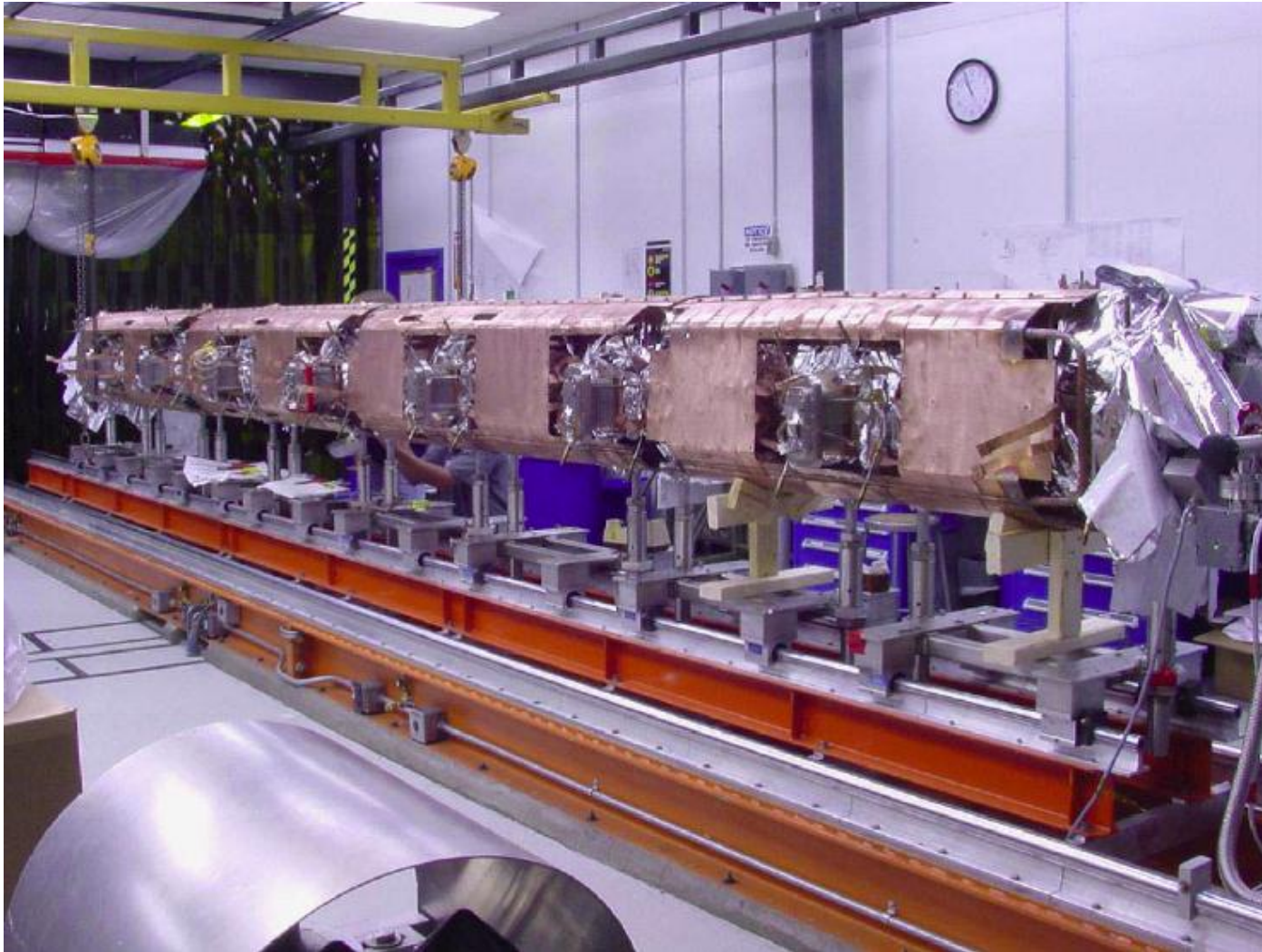
# Cm in Test Cave



# CEBAF Upgrade



# CEBAF Upgrade



# CEBAF Upgrade

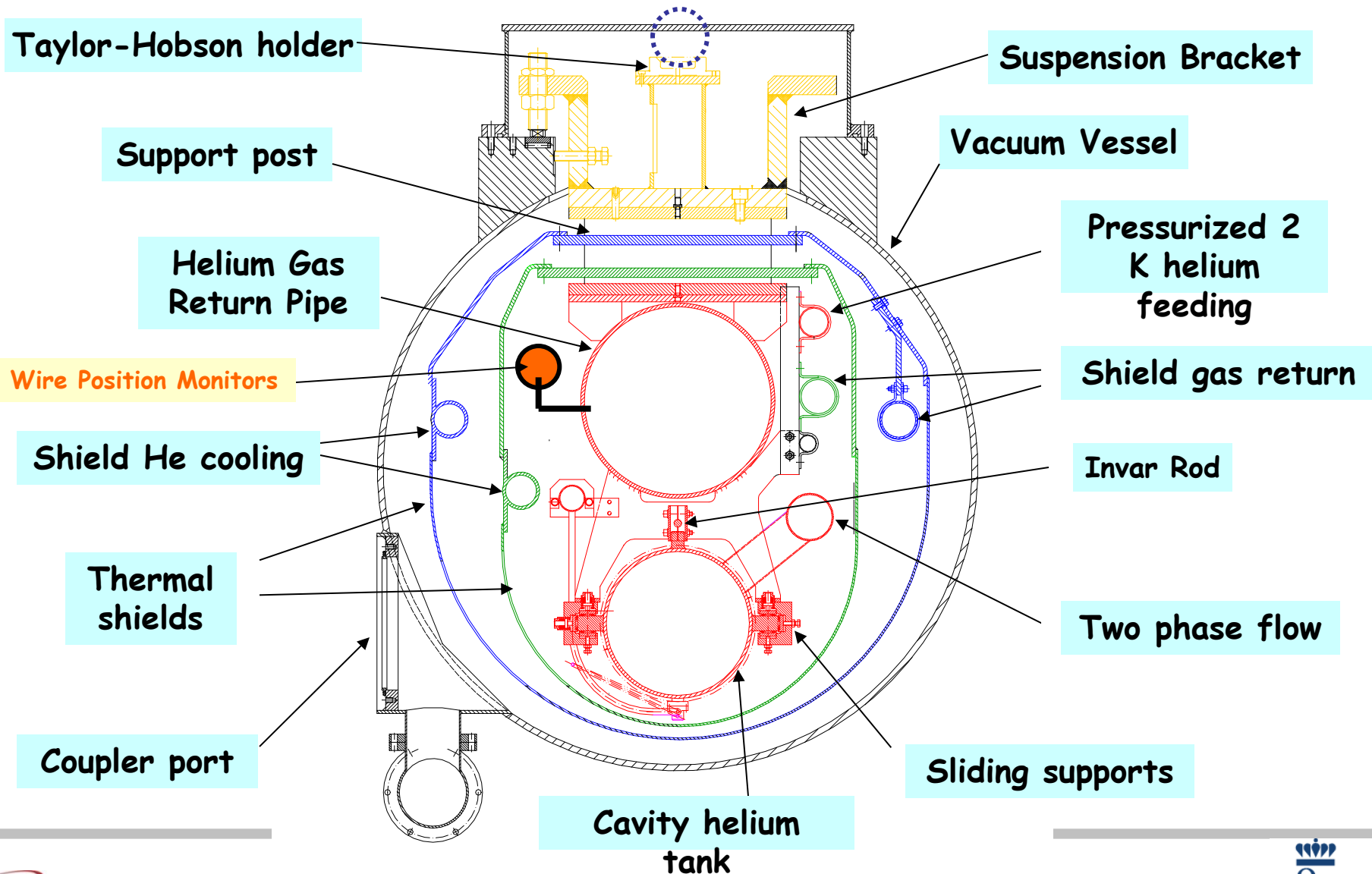




# CEBAF Upgrade

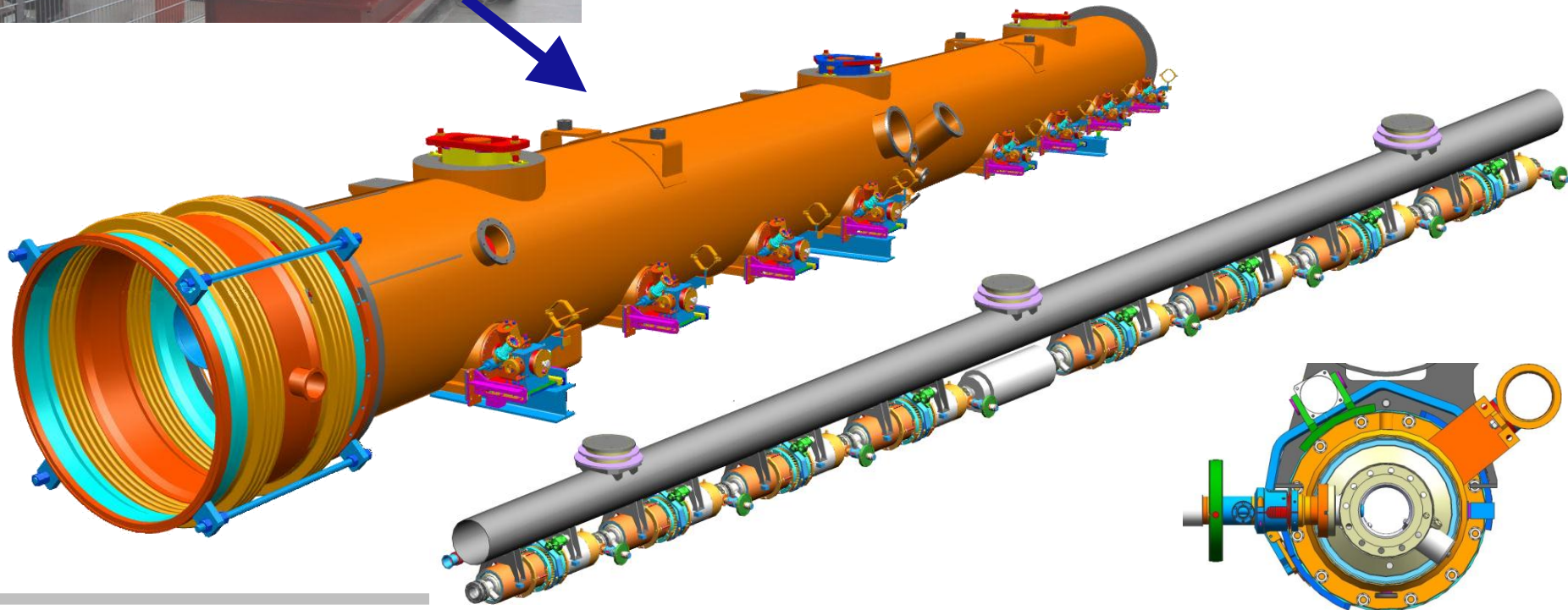
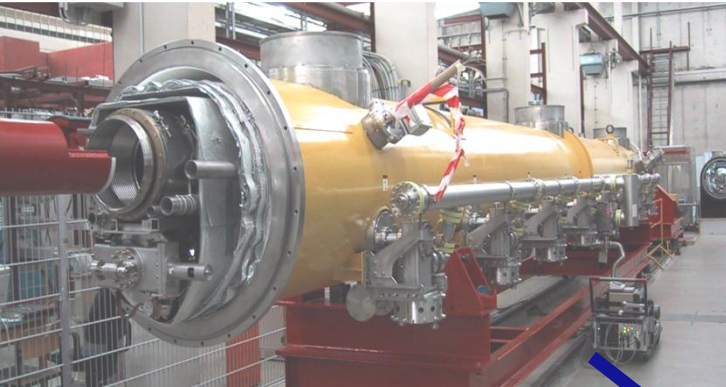


# Detailed Cry 3 Cross Section

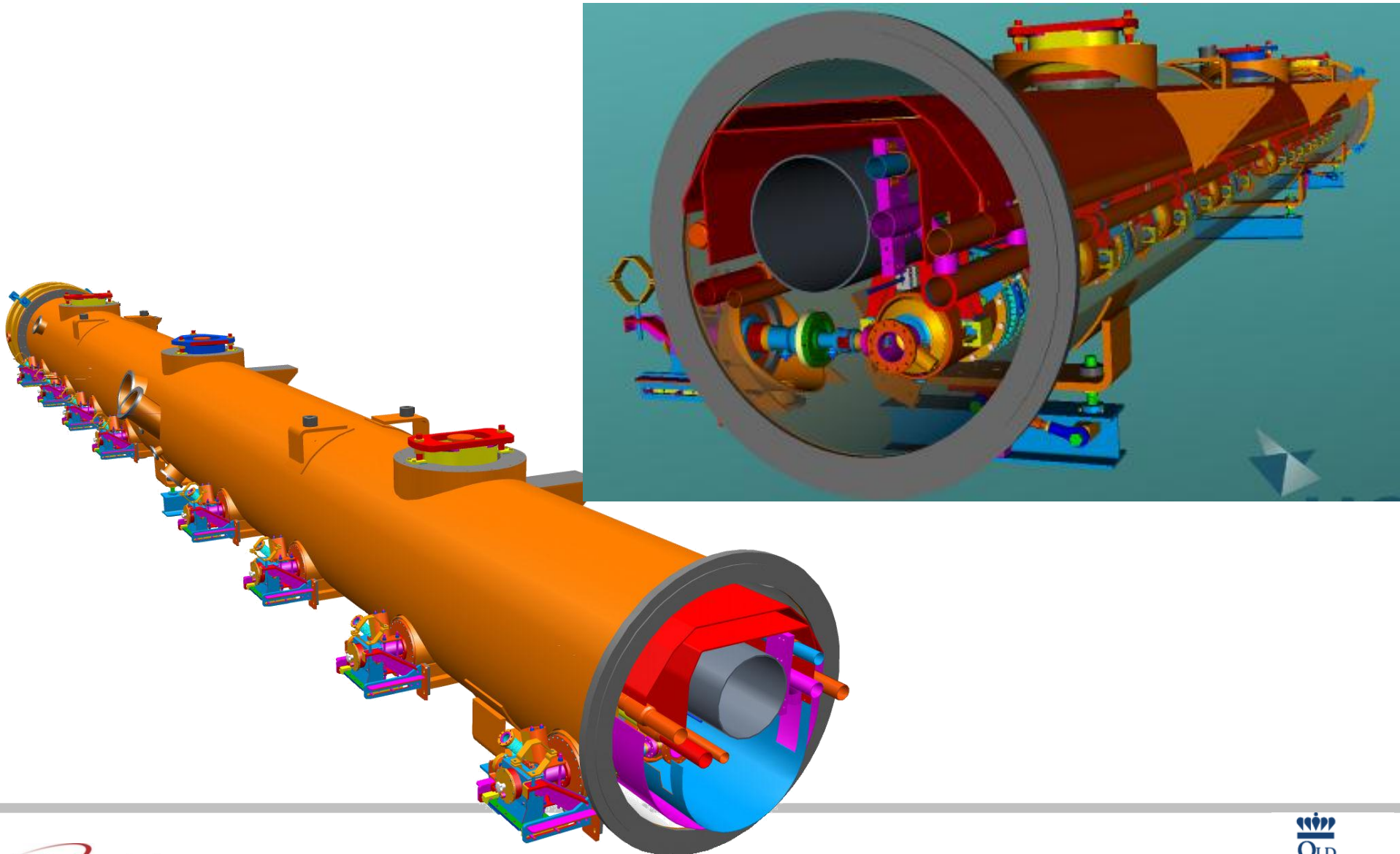


# Towards ILC Cryomodule

- International collaborative Effort in the three regions
- Design changes are towards nailing down slot length of components
  - Costing should be straight-forward from TTF (and possibly XFEL) experience



# ILC Cryomodule: Conceptual Model



# Module assembly picture gallery - 1



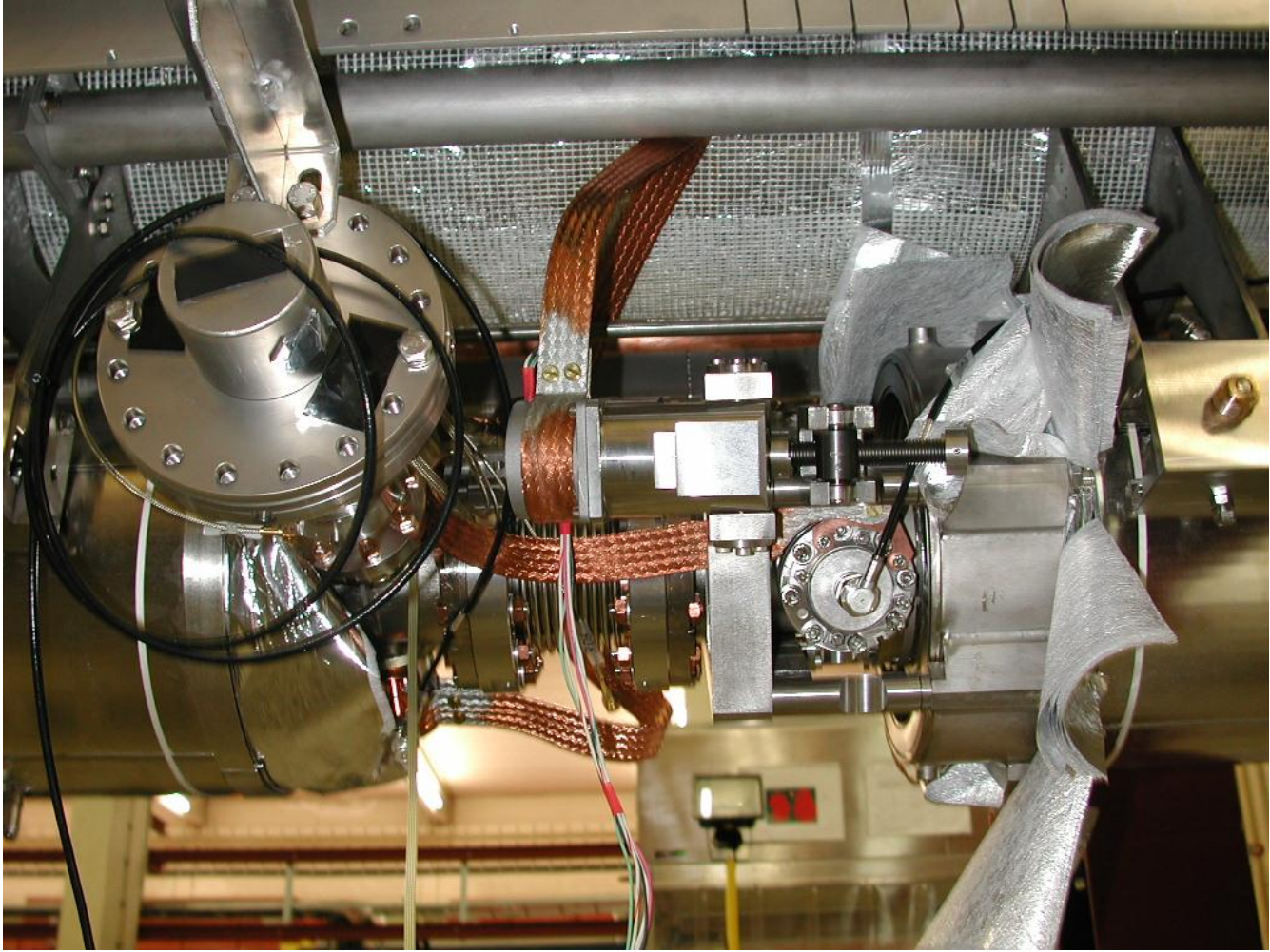
String inside the Clean Room

# Module assembly picture gallery - 2



String in the assembly area

# Module assembly picture gallery - 3



Cavity interconnection detail

# Module assembly picture gallery - 4



String hanged to he HeGRP



# Module assembly picture gallery - 5



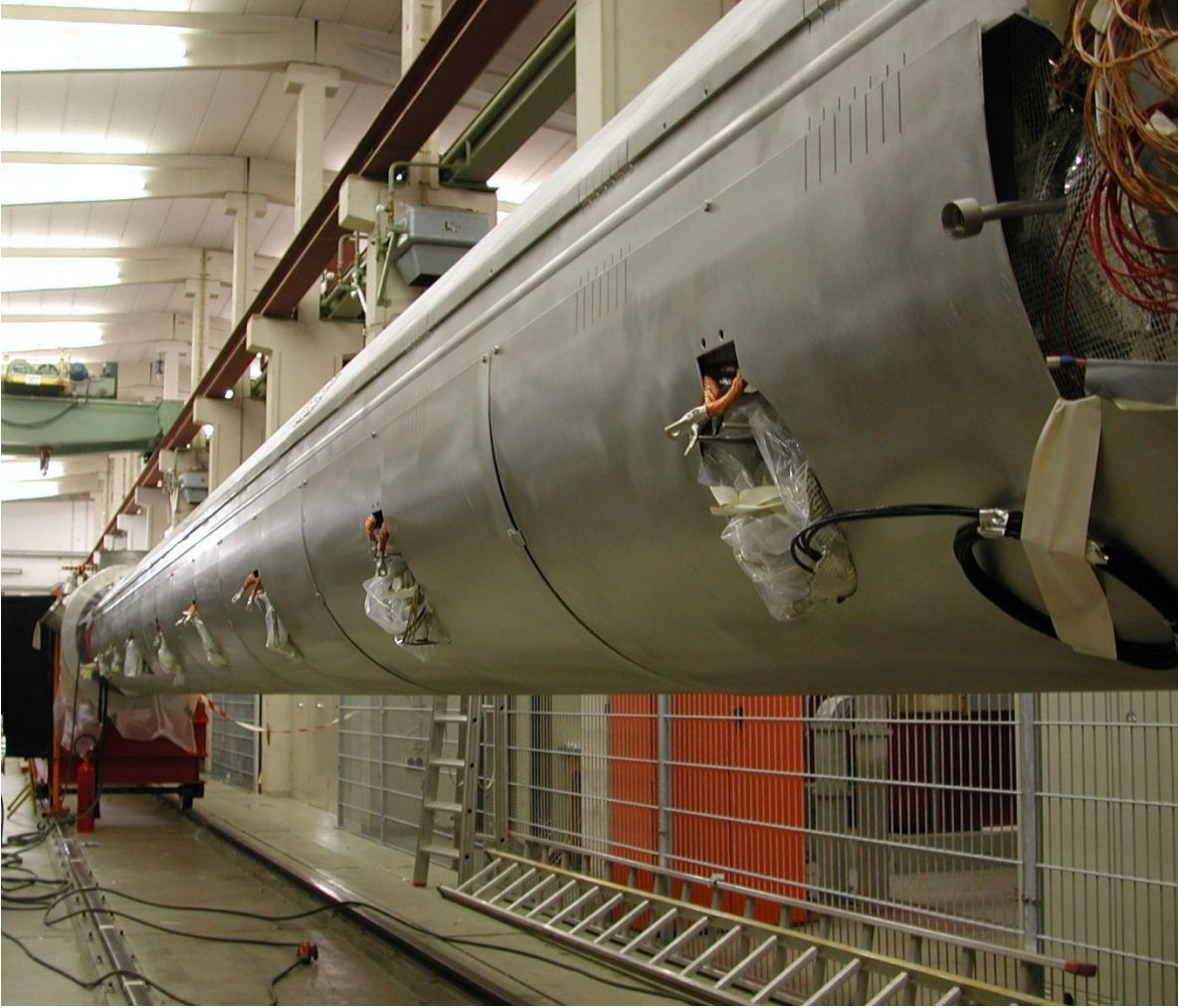
String on the cantilevers

# Module assembly picture gallery - 6



Close internal shield MLI

# Module assembly picture gallery - 7



External shield in place

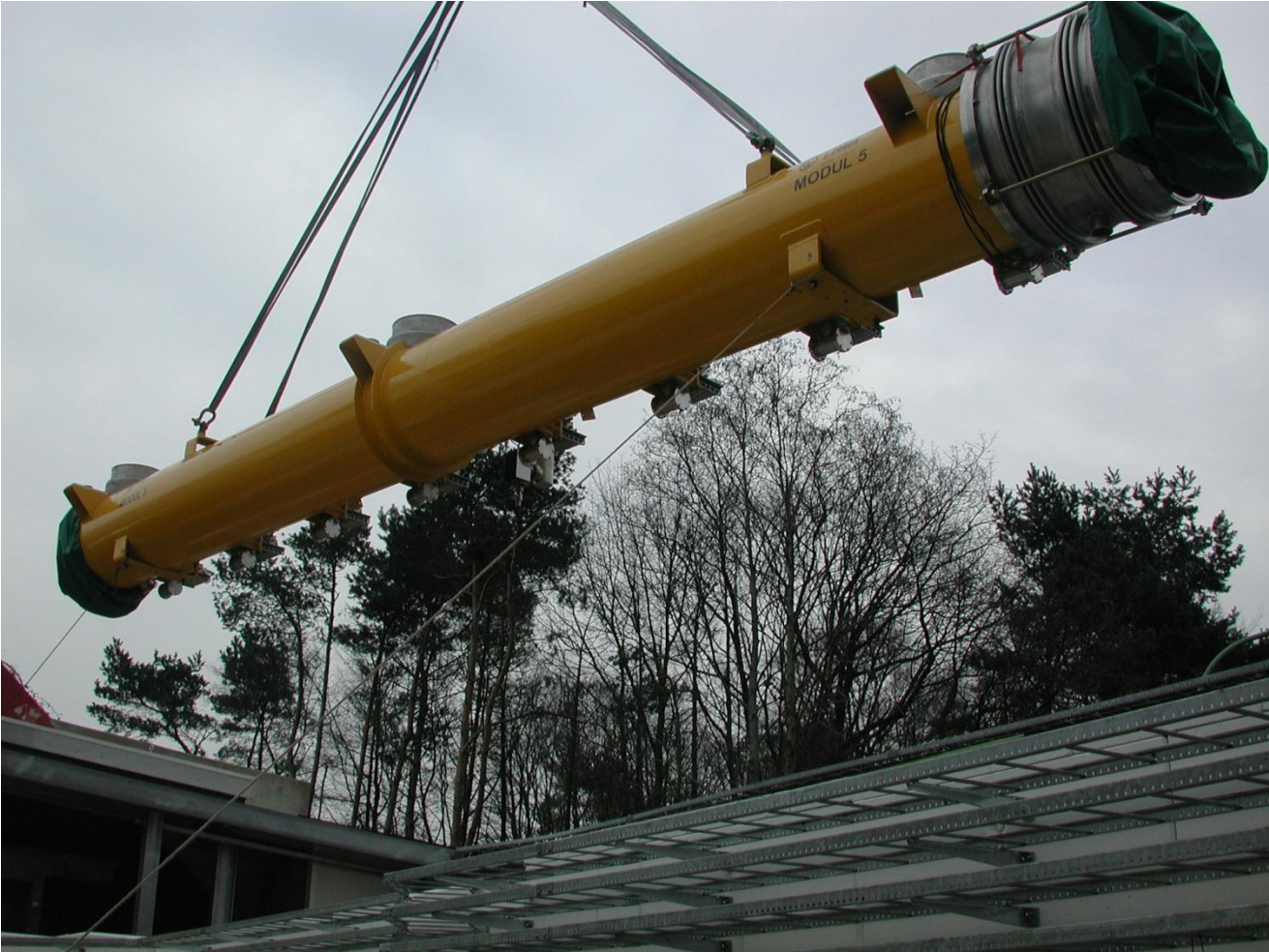


Welding "Fingers"



Sliding VV on shield (MLI)

# Module assembly picture gallery - 8



Complete module moved for storage

# The Soleil Cryomodule

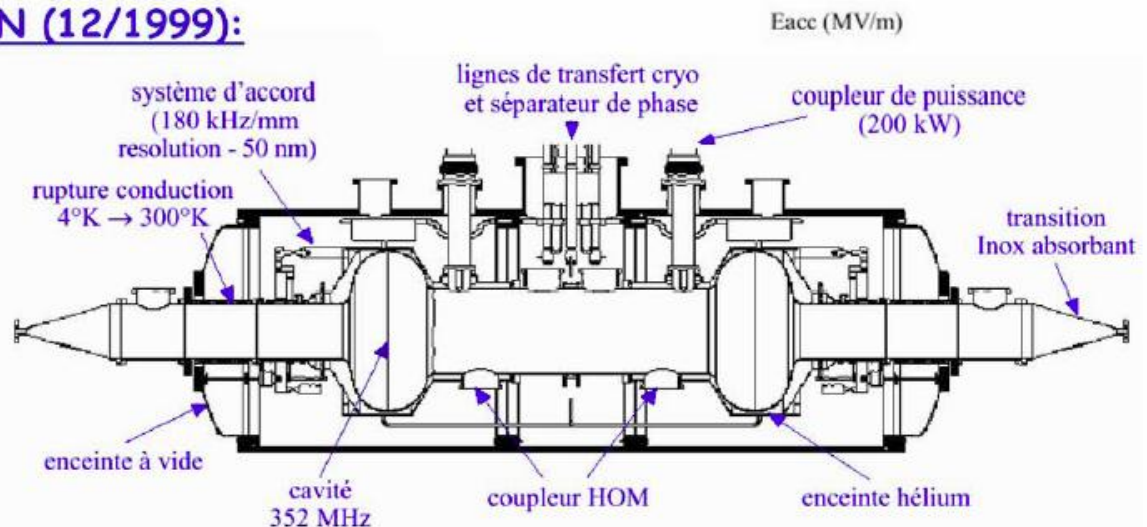
2.75 GeV, 500 mA Light Source

## Design Parameters

- Nb/Cu single-cell HOM damped cavities
- Designed and built by Saclay/CERN collaboration
- 352 MHz
- 2 two-cavity cryomodules
- 1.2 MV/cavity
- LEP input couplers @ 200 kW
- loop HOM couplers
- Static heat loss 42 W

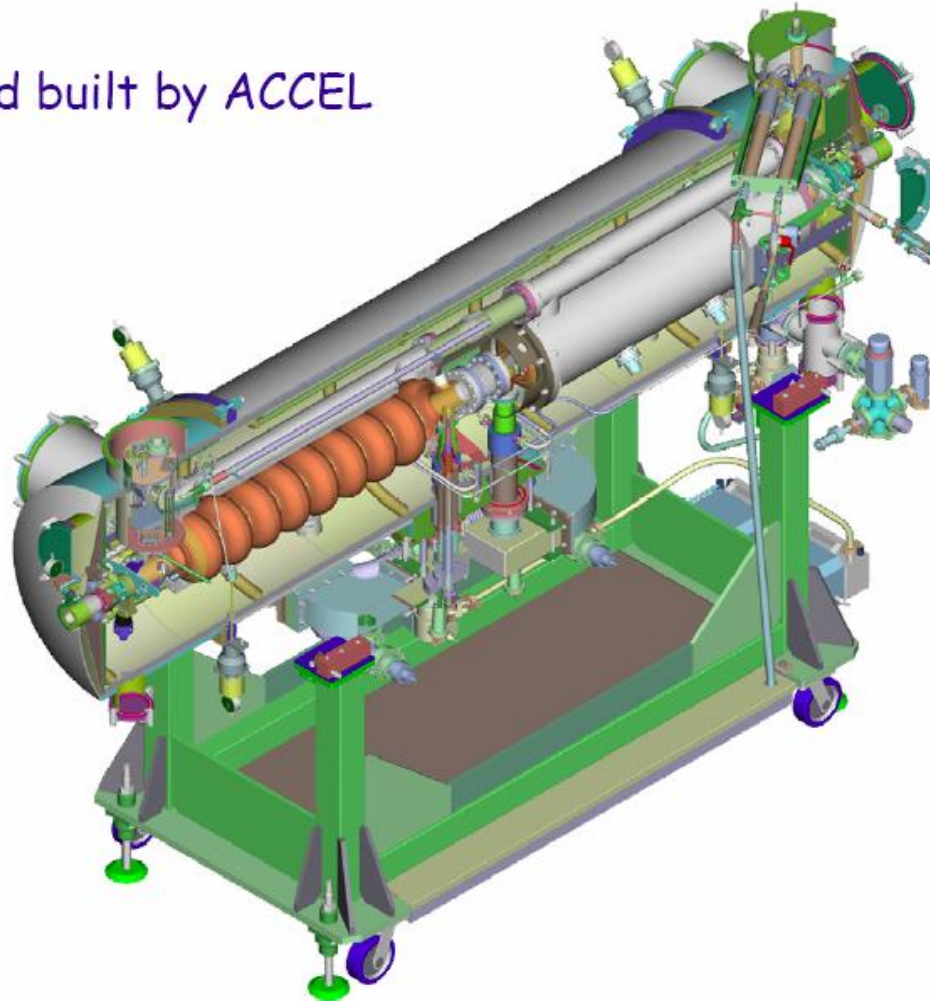
## High power test at CERN (12/1999):

- $E_{acc}$  up to 7 MV/m
- 120 kW RF power
- 20 W static heat leak
- Not optimal  $Q_{ext, fund}$  of dipole HOM couplers



# The Rossendorf Cryomodule

Designed and built by ACCEL



# The CESR Cryomodule



# ATLAS - ANL





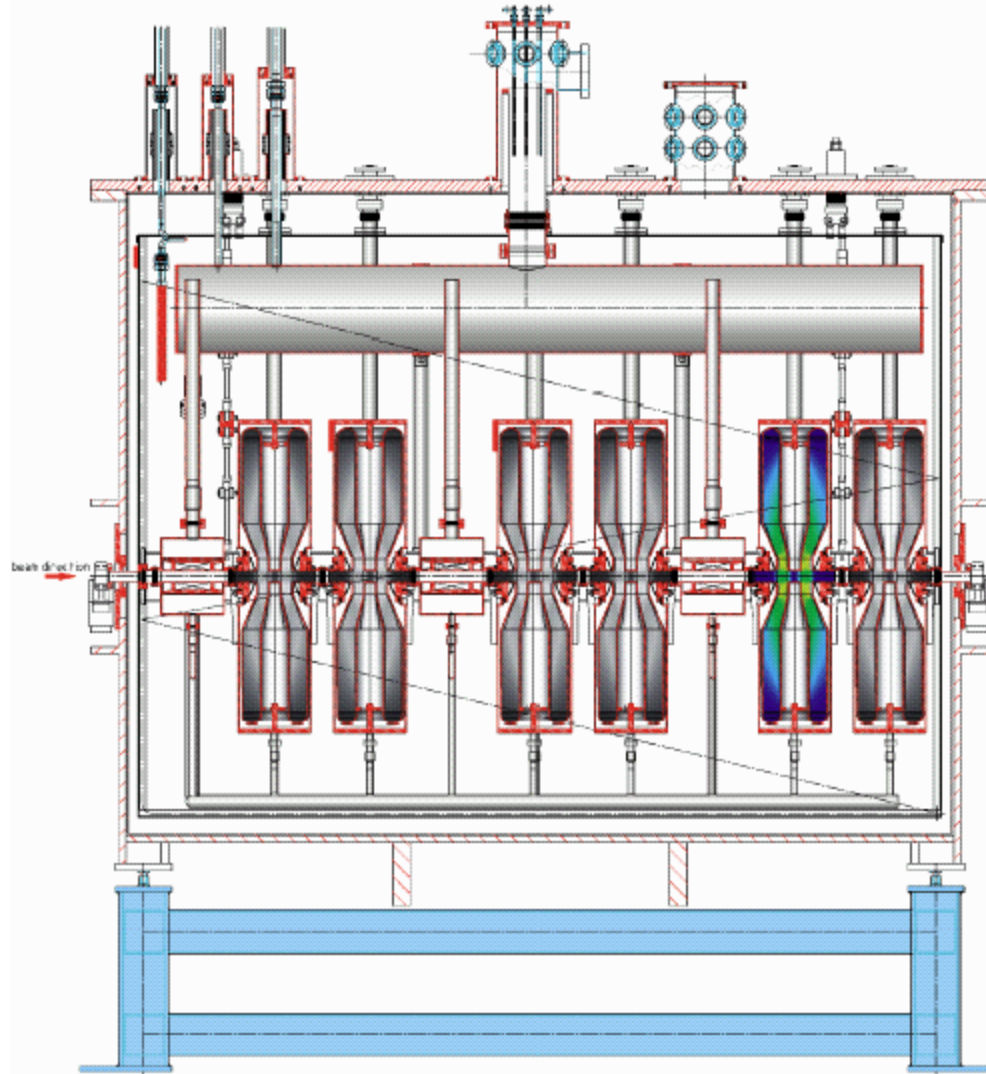
# JAERI



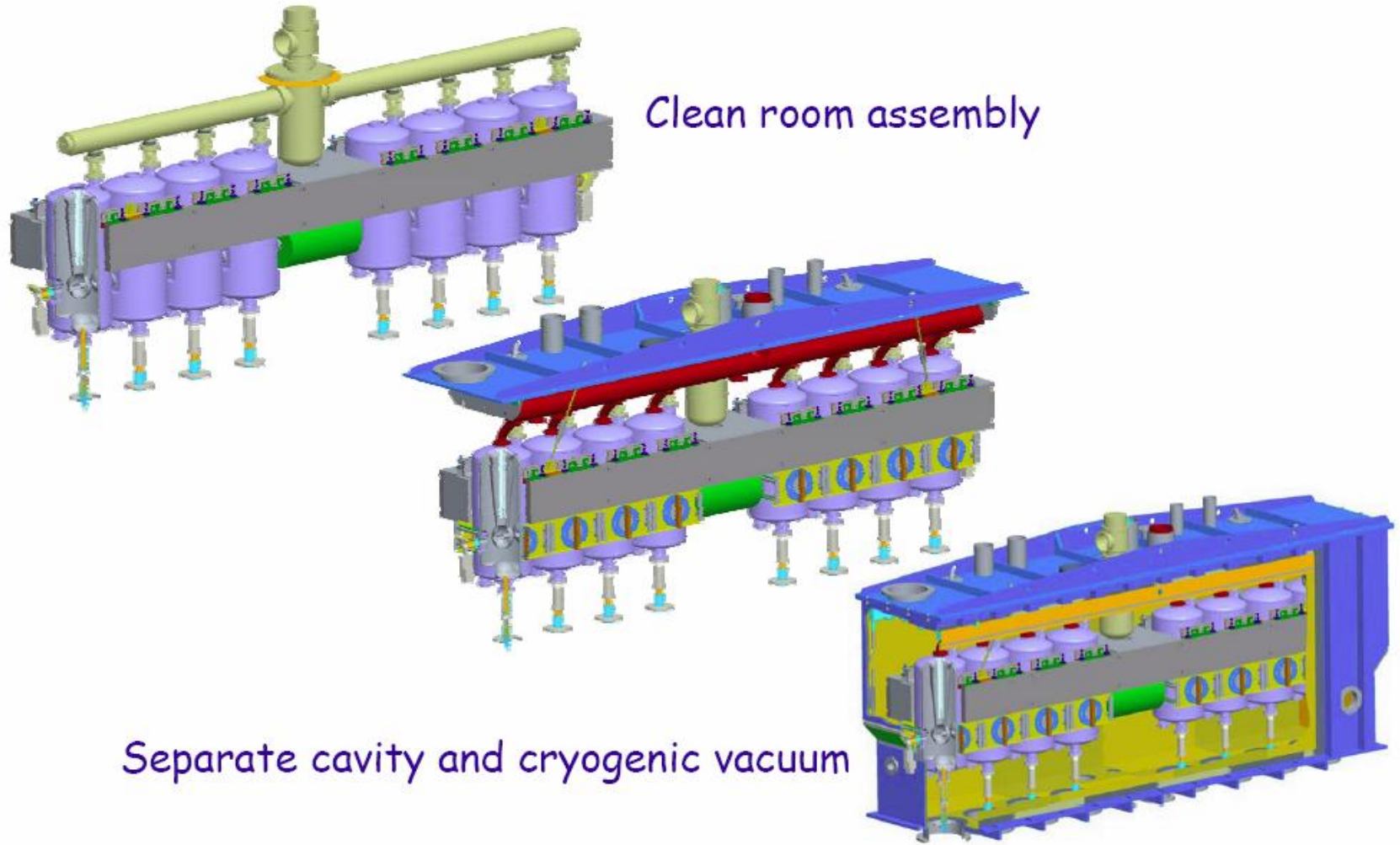
# ALPI - LNL



# SARAF (Accel)

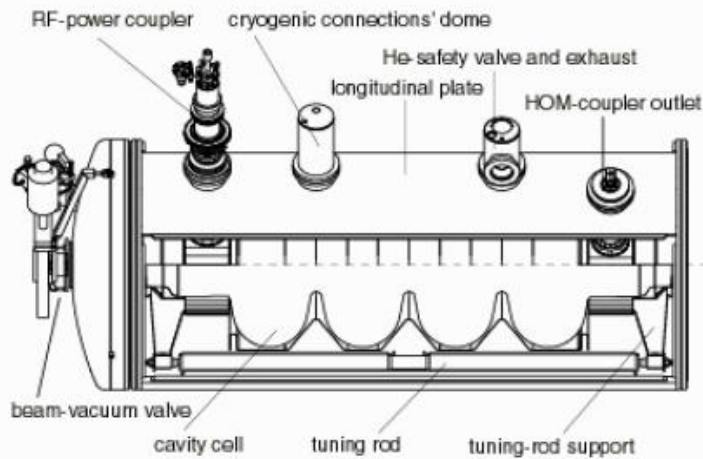
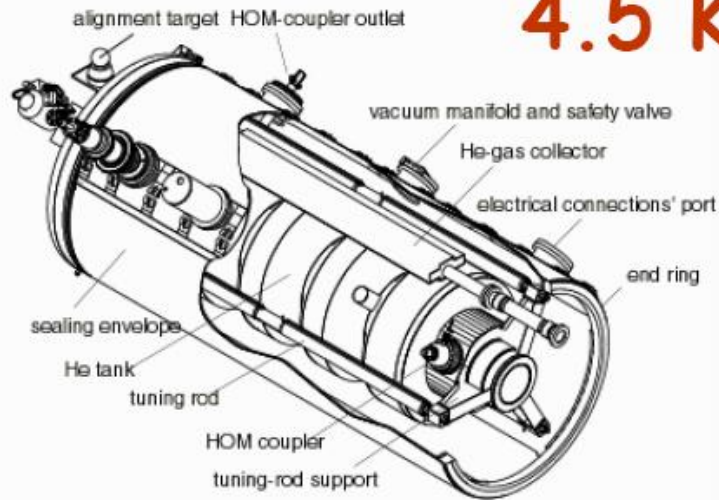


# ANL

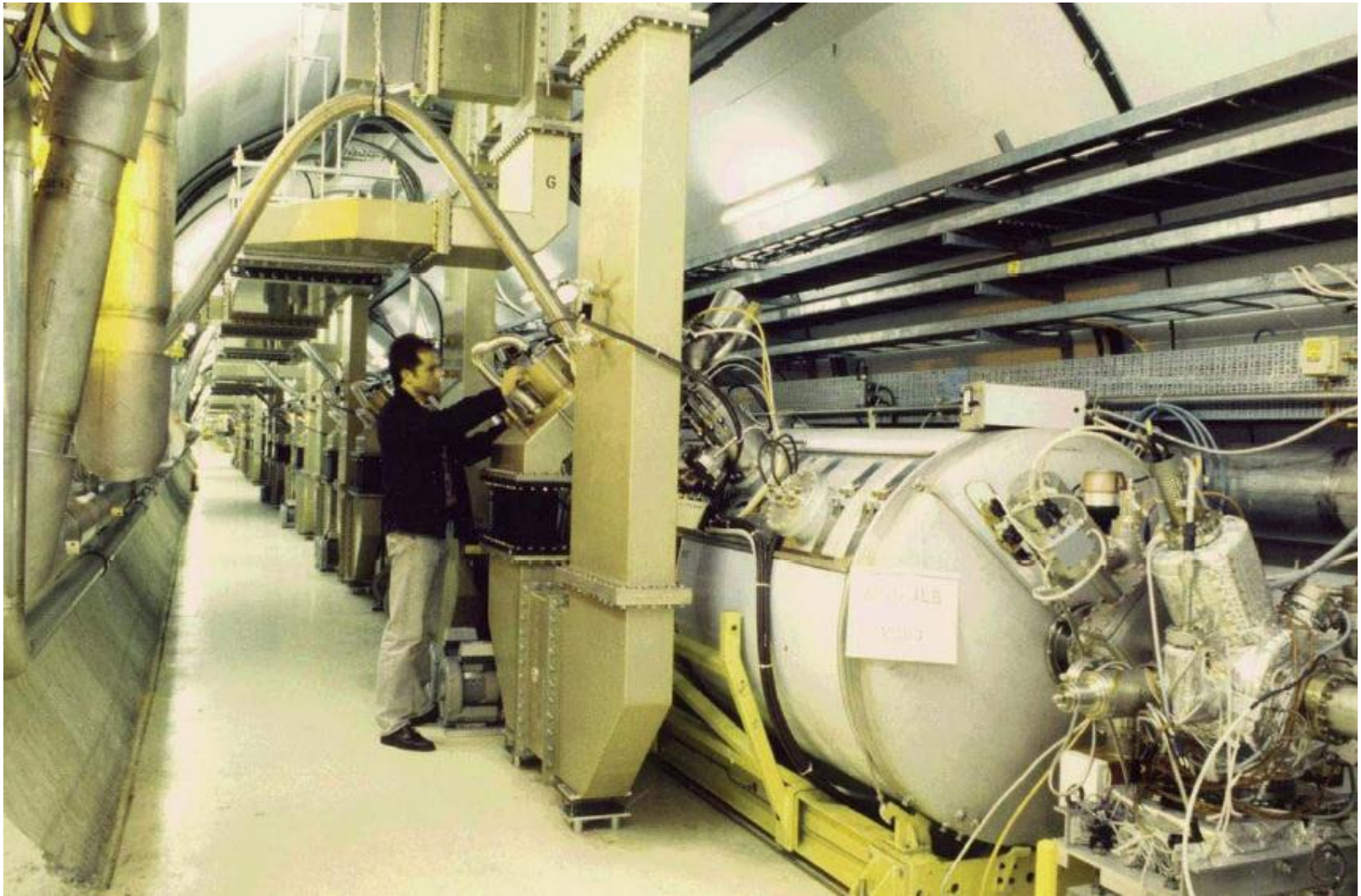


# LEP II

## 4.5 K



# LEP II



# HERA

