



Imaging a Beam with Synchrotron Light

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- A later lecture derives the spectrum of synchrotron radiation from a highly relativistic electron. For now, a few results:
 - Power radiated while traveling along an orbit with radius of curvature ρ

$$P_s = \frac{2}{3} \frac{\gamma^4 r_e m_e c^3}{\rho^2}$$

where the "classical electron radius" is $r_e = \frac{e^2}{4\pi\varepsilon_0 m_e c^2} = 2.818 \times 10^{-15} \text{ m}$

• The factor of γ^4 makes this power substantial. For example, 2 A of 9-GeV electrons in the PEP-II high-energy ring (HER) radiate

$$P_s I_{\rm HER}/ec = 6.8 \text{ kW/m}$$

in the dipole magnets. The total power lost around the whole ring is

$$2\pi\rho_{\rm HER} P_s I_{\rm HER} / ec = 7.0 \,\rm MW$$

where $\rho_{\text{HER}} = 165$ m in the 192 arc dipoles.

• Power per unit frequency ω and solid angle Ω

$$\frac{d^{2}P}{d\Omega d\omega} = \frac{\gamma P_{s}}{\omega_{c}} F_{s}(\omega, \psi) = \frac{\gamma P_{s}}{\omega_{c}} \left[F_{s\sigma}(\omega, \psi) + F_{s\pi}(\omega, \psi) \right]$$

• where the terms give the power in the two polarization components:

- $F_{s\sigma}$: In the plane of the bend (typically the horizontal plane)
- $F_{s\pi}$: Perpendicular to the bend plane (and so typically vertical)

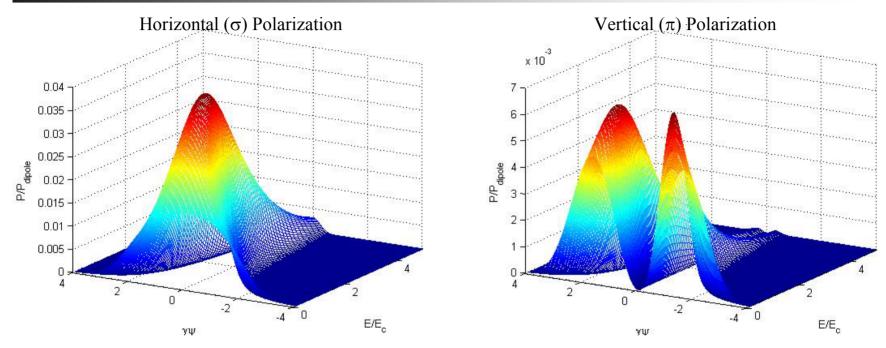
$$F_{s\sigma} = \left(\frac{3}{2\pi}\right)^3 \left(\frac{\omega}{2\omega_c}\right)^2 \left(1 + \gamma^2 \psi^2\right)^2 K_{\frac{2}{3}}^2 \left[\frac{\omega}{2\omega_c} \left(1 + \gamma^2 \psi^2\right)^{\frac{3}{2}}\right]$$
$$F_{s\pi} = \left(\frac{3}{2\pi}\right)^3 \left(\frac{\omega}{2\omega_c}\right)^2 \gamma^2 \psi^2 \left(1 + \gamma^2 \psi^2\right) K_{\frac{1}{3}}^2 \left[\frac{\omega}{2\omega_c} \left(1 + \gamma^2 \psi^2\right)^{\frac{3}{2}}\right]$$

• ψ is the vertical angle, and $K_{1/3}$ and $K_{2/3}$ are modified Bessel functions.



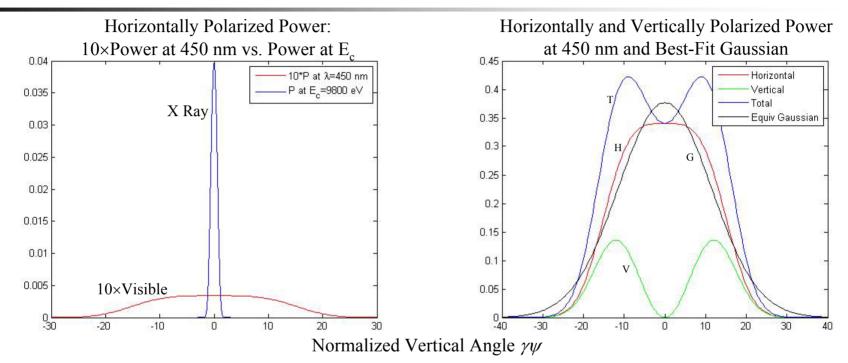
- The "critical energy" is $E_c = \hbar \omega_c = \frac{3}{2} \gamma^3 \hbar \frac{c}{\rho}$
 - ω_c is the revolution frequency c/ρ , but scaled by γ^3 .
 - This large factor moves the frequency from MHz to x-rays.
 - For PEP's HER dipoles, $E_c = 9.8$ keV.
- Half of the total energy is below E_c , half above.
 - Almost all power is emitted as hard photons.
 - Visible light is far into the tail.





- The peak of the horizontal is 6 times higher than the vertical.
 This peak is a little below the critical energy.
- The vertical component is zero on the midplane ($\psi = 0$).
 - Symmetry: No preference for upward versus downward field.
- The range of angles spanned is much wider at low energies.





• Power in visible is much weaker and broader than for x rays (above left, for HER).

- For x rays ($E \sim E_c$), the angular width (the "opening angle") is roughly $1/\gamma$.
- For visible $(E \ll E_c)$, a Gaussian approximation (above right) to the horizontal polarization has an RMS width of: $\sigma_{\psi} \approx \frac{0.75}{\gamma} \left(\frac{E_c}{E}\right)^{\frac{1}{3}}$
- Horizontally polarized power is roughly Gaussian, but with flatter top, smaller tails.
 - Area of horizontal is 3 times area of vertical.

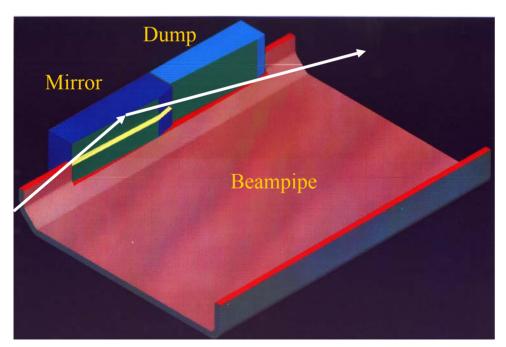
- Typical imaging situation:
 - Object reflects unpolarized incident light in all directions.
 - Lens catches some light from almost any angle.
 - Most objects have more transverse extent than depth.
- Synchrotron Light:
 - The source of the light is the object's own emission.
 - Light is radiated only in the forward direction, tangent to the beam's instantaneous circular path through a bend.
 - Vertically: The beam lights up narrow forward-directed cone.
 - Horizontally: The beam paints a stripe of light along the midplane of the vacuum chamber as bends.
 - Like a car rounding a bend in the dark with its bright headlights on.
 - Longitudinal profile is Gaussian at any instant.
 - But over the exposure time, the source goes around the ring many times.
 - We want to measure a glowing, curved string by imaging it from a tangent.

- Visible light has advantages (in addition to being easy to see):
 - You can use common parts like windows, lenses, mirrors, video cameras, and specialized instruments like streak cameras.
 - The wide opening angle is wider than at the critical wavelength.
 - Remove the narrow fan with most of the heat, without much loss to the visible image, in order to avoid thermal distortion of the first mirror (M1).
 - "Cold finger": a narrow cooled mask on the midplane, upstream of M1, that blocks the x-ray fan while casting a thin shadow across the mirror.
 - Slot along the middle of M1, so that the x-rays pass through and can't heat it.
 - A thin, low-Z substrate (beryllium) for M1, to transmit most of the x-rays.
- But diffraction limits the resolution at longer wavelengths.
 - An important consideration when the beam is small.
 - Image a point near a defocusing quad, where the beam is large vertically.
 - A cold finger or slot also adds diffraction.
 - Drives the design toward shorter wavelengths.
 - At least blue rather than red, but sometimes ultraviolet or x rays.



Slotted First Mirror in PEP-II

- Midplane slot allows x-ray fan to bypass
 M1 and strike the thermal dump.
 - But slot is a mechanical weak point.
 - PEP's x-ray fan is very narrow and hot, making a cold finger difficult.







"Cold Finger" Mask in SPEAR-3

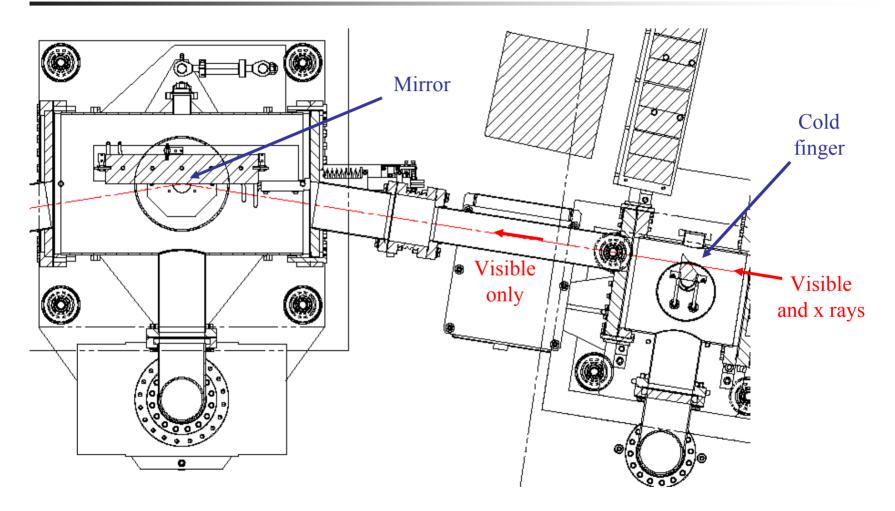
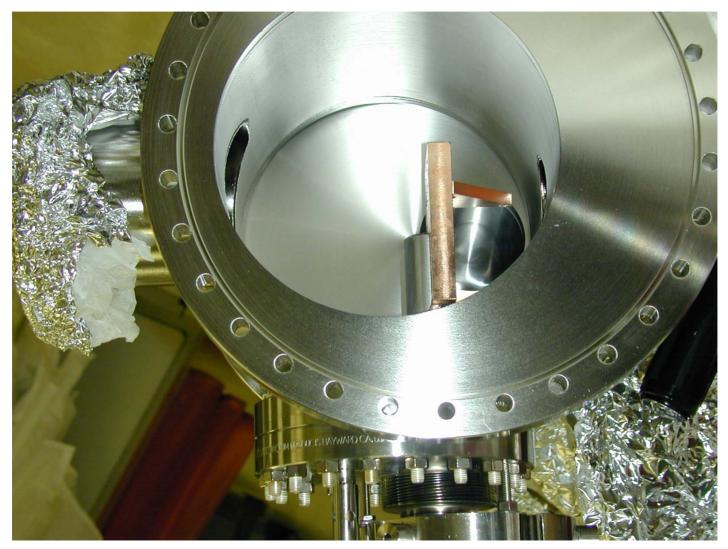
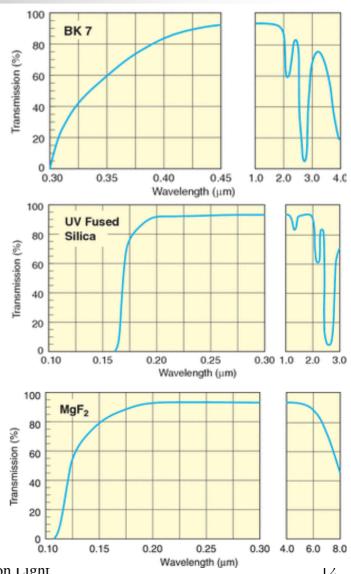




Photo of Cold Finger in SPEAR-3



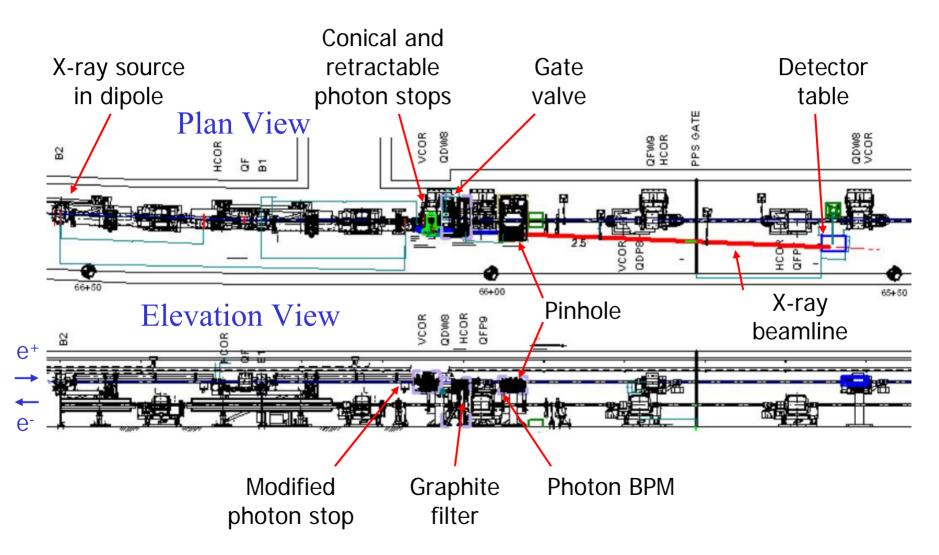
- Can't go far into the UV without problems.
 - Window and lens materials become opaque:
 - Glasses (like BK7 at right) are useful above ~330 nm.
 - Fused silica works above ~170 nm.
 - Special materials like MgF₂ work above $\sim 120 \text{ nm}$
 - Absorption in air below ~100 nm
 - Must use reflective optics in vacuum.



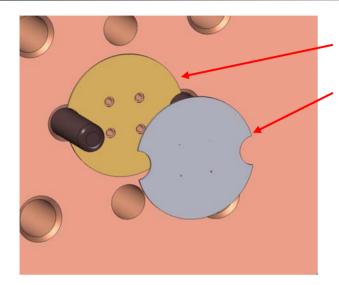


- The good news: Most of the beam's emission is in the x-ray range.
- The bad news: How do you form an image?
 - You can use a simple pinhole camera.
 - But this throws out most of the light.
 - Must absorb this power before the pinhole, or it will get too hot.
 - Other imaging optics are difficult:
 - Grazing-incidence optics
 - Zone plates

X-Ray Pinhole Camera in the PEP-II LER

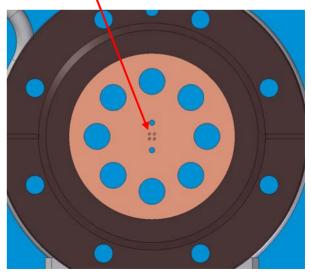


Design of the Pinhole Assembly



- Gold disk for heat transfer
- Pt:Ir (90:10) disk with 4 pinholes.
 - Diameters of 30, 50, 70, and 100 μm.
- Front: Glidcop with 4 larger holes

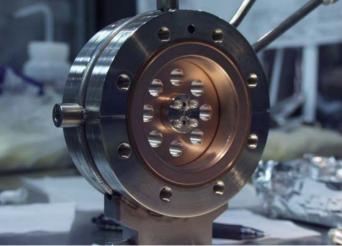




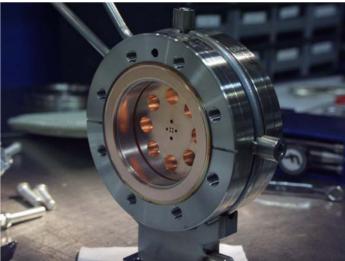


Photos of the Pinhole Assembly

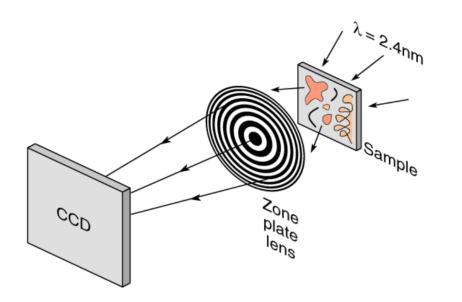


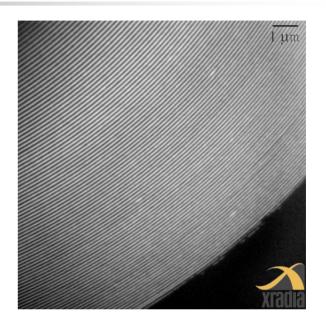






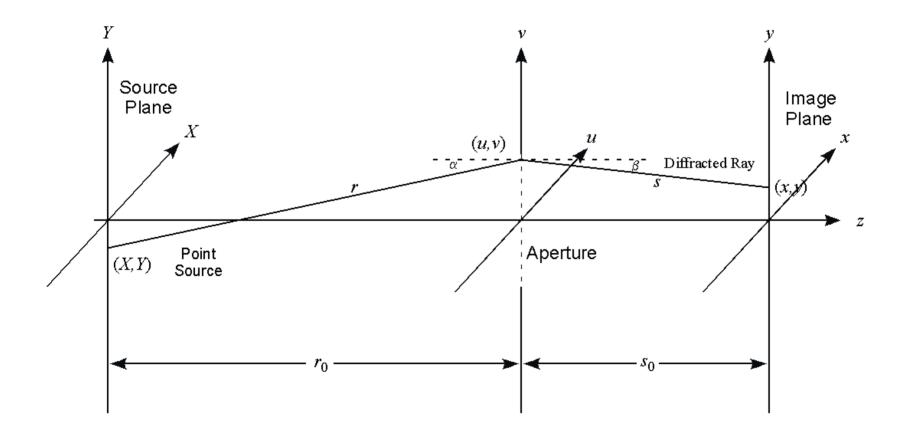






- A diffractive lens, made by lithography
- High-Z metal (gold) on thin membrane of low Z (SiN)
- Requires low power and a narrow bandwidth ($\approx 1\%$)
 - Precede with a pair of multilayer x-ray mirrors, for narrow-band reflection and for absorption of out-of-band power.







- All points in an aperture are considered point sources, reradiating light incident from a point source
 - Wavelength is $\lambda = 2\pi/k$.
- The field at (x,y) is given by a Fresnel-Kirchhoff integral over the (small) aperture:

$$E(x, y) = -\frac{Ai}{2\lambda} \iint_{\text{aperture}} \frac{e^{ik(r+s)}}{rs} (\cos \alpha + \cos \beta) dS$$
$$\approx -\frac{Ai}{2\lambda r_0 s_0} (\cos \alpha + \cos \beta) \iint_{\text{aperture}} e^{ik(r+s)} dS$$

• Everything is essentially constant except the phase from each point in the aperture.



$$r = \sqrt{(X-u)^{2} + (Y-v)^{2} + r_{0}^{2}} \approx r_{0} + \frac{(X-u)^{2} + (Y-v)^{2}}{2r_{0}}$$

$$s = \sqrt{(x-u)^{2} + (y-v)^{2} + r_{0}^{2}} \approx s_{0} + \frac{(x-u)^{2} + (y-v)^{2}}{2s_{0}}$$

$$e^{ik(r+s)} \approx \exp\left[ik\left(r_{0} + s_{0} + \frac{X^{2} + Y^{2}}{2r_{0}} + \frac{x^{2} + y^{2}}{2s_{0}}\right)\right] \exp\left[ik\left(\frac{u^{2} + v^{2}}{2r_{0}} + \frac{u^{2} + v^{2}}{2s_{0}}\right)\right] \exp\left[-ik\left(\frac{Xu + Yv}{r_{0}} + \frac{xu + yv}{s_{0}}\right)\right]$$

- First term: Independent of the aperture coordinates *u*, *v*.
 - Contributes only an overall phase to the *uv* integral over the aperture.
- Second: Small (since aperture is small) quadratic terms in *u*, *v*.
- Third: Products of u, v with cosines (X/r_0 , etc.) of ray angles from the source or measurement points to the x and y axes.
 - The only term that matters in the integral over the aperture is:

$$e^{ik(r+s)} \approx \exp\left[-ik\left(pu+qv\right)\right]$$

where $p = X/r_0 + x/s_0$ and $q = Y/r_0 + y/s_0$

Fisher — Imaging with Synchrotron Light

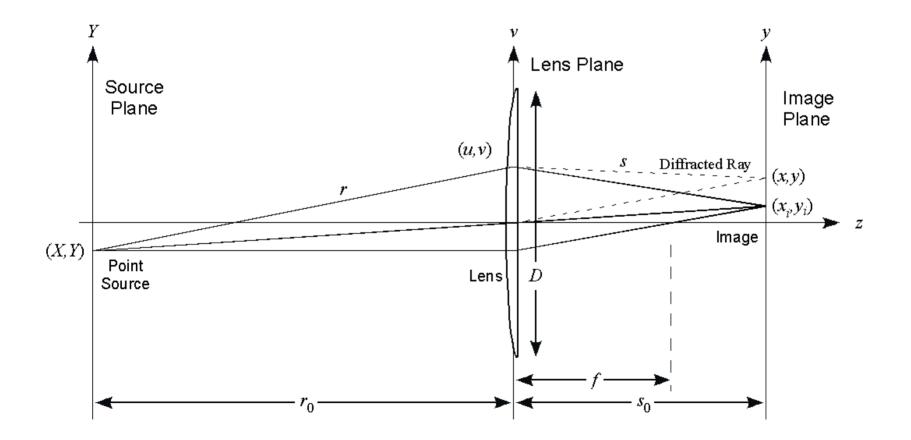
Spatial Fourier Transform

• The diffraction pattern on the *xy* plane becomes a Fourier transform in the spatial coordinates *uv* of the aperture:

$$E(x,y) = -\frac{Ai}{2\lambda r_0 s_0} (\cos\alpha + \cos\beta) \iint_{\text{aperture}} e^{-ik(pu+qv)} dudv$$

- Laser light is sometimes focused through a pinhole to remove noisy, non-Gaussian parts of the transverse profile.
 - The hole forms a *spatial filter*: since the noise is found at high *spatial frequencies*, which appear at larger values of *u* and *v*, it can be clipped by a properly sized hole.





- All paths from source (X, Y) to image (x_i, y_i) have *equal* length.
 - A fundamental property of geometric imaging.
 - The phase difference in the uv integral arises from the different paths from (X,Y) to (x,y), compared to the equal paths from (X,Y) to (x_i,y_i) .
 - It is helpful to subtract this reference path, so that the phase difference becomes the difference between (u,v) to (x,y) and (u,v) to (x_i,y_i) .

$$\sqrt{(x-u)^2 + (y-v)^2 + s_0^2} - \sqrt{(x_i - u)^2 + (y_i - v)^2 + s_0^2}$$

$$\approx -\frac{(x-x_i)u + (y-y_i)v}{s_0} = -\frac{\rho w}{s_0} \cos(\phi - \psi)$$

• Here we used polar coordinates: $(u,v) \rightarrow (w,\psi)$ and $(x-x_i,y-y_i) \rightarrow (\rho,\phi)$



• The diffraction integral (neglecting constants) becomes:

$$E(x,y) = \int_0^{2\pi} \int_0^{D/2} \exp\left[-ik\frac{\rho w}{s_0}\cos(\phi - \psi)\right] w dw d\psi$$
$$= 2\pi \int_0^{D/2} J_0\left(\frac{k\rho w}{s_0}\right) w dw = \left(\frac{\pi D^2}{4}\right) \frac{2J_1\left(\frac{k\rho D}{2s_0}\right)}{\frac{k\rho D}{2s_0}}$$

where we have used two Bessel-function identities.This is called the Airy diffraction pattern.

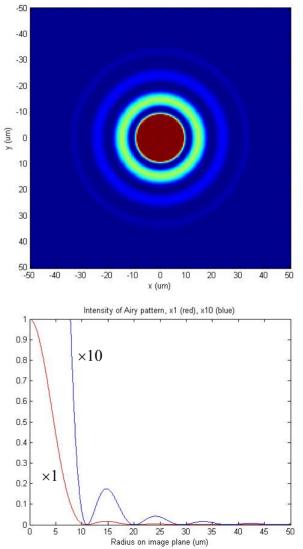


Diffraction by a Lens: Airy Pattern

• Concentric circles, with the first minimum at radius r_A :

$$r_A = 1.22\lambda \frac{L}{D} = 1.22F\lambda = 0.61\frac{\lambda}{\theta}$$

- *F* is called the "F-number" of the lens.
- θ is the half angle of the light cone illuminating the lens.
- Plot for $\lambda = 450$ nm, D = 50 mm, $s_0 = 1$ m
 - The central circle at right is saturated by a factor of 30 to highlight the faint rings.
 - The plot is expanded by 10 to show the rings.
- r_A is the resolution of the imaging system.
 - Compare it to the size of the geometric image to see if diffraction is a problem.



• Approximating the half angle θ with 1 to 2 times the Gaussian angle σ_{ψ} gives a resolution (neglecting factors of order unity) of:

$$r_{SR} \approx 0.5 \frac{\lambda}{\sigma_{\psi}} \approx \rho^{\frac{1}{3}} \lambda^{\frac{2}{3}}$$

- A difficult case: The HER of PEP-II has $\rho = 165$ m. For blue light at 450 nm, this resolution is $\rho^{\frac{1}{3}}\lambda^{\frac{2}{3}} = 0.32$ mm
- A more thorough treatment substitutes the SR power spectral density from the point source into a Fraunhofer diffraction integral over the area of the lens illuminated through the beamline aperture, finding the field at (x',y') on the image.

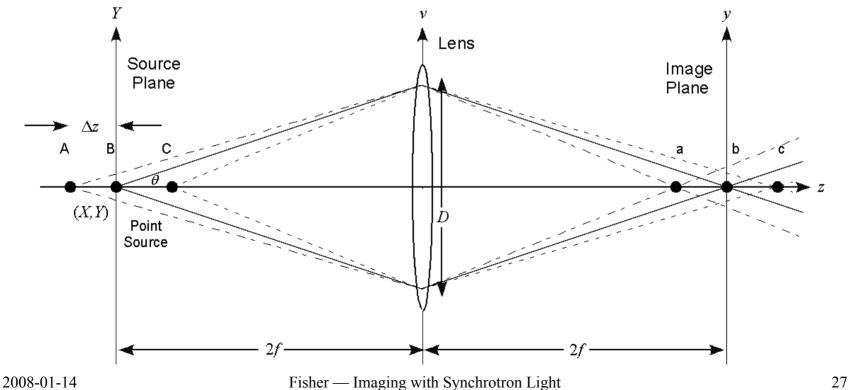
$$E(x', y') = A \int_{-x_a}^{x_a} dx \int_{-\infty}^{\infty} dy \frac{\gamma P_s}{\omega_c} F_s(\omega, \psi) e^{-ik(u'x + v'y)}$$

with $k = 2\pi/\lambda$ $u' = x'/L'$ $v' = y'/L'$

• The first minimum of the intensity then gives the resolution.



- Our light source is a long, gradual arc, not a plane.
 - What is the source distance?
 - Can it all be in focus?
 - How do you avoid blurring the measurement?





• Diameters of A and C images as they cross the *xy* plane, based on typical rays at angles $\pm \theta/2$:

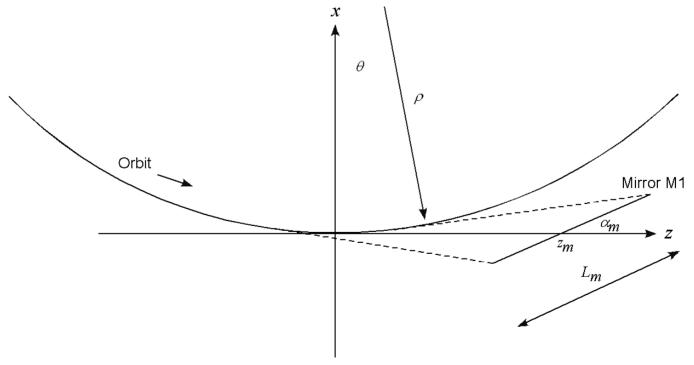
$$d = 2 \left| \frac{D/4}{2f \mp \Delta z} (\pm \Delta z) \right| \approx \frac{D\Delta z}{4f} = \theta \Delta z$$

- The vertical angle θ lighting the lens is roughly $2\sigma_{\psi}$.
- If we capture a similar portion of a horizontal arc:

$$\Delta z = \rho \sigma_{\psi}$$
$$d = \theta \Delta z = 2\rho \sigma_{\psi}^{2} = 0.4\rho^{\frac{1}{3}}\lambda^{\frac{2}{3}}$$

- This expression is similar to the diffraction resolution.
- But how much of the orbit do we actually capture?

- Consider the beam's orbit both in the horizontal plane (xz) and in horizontal *phase space* (xx').
 - x' is the beam's angle to the direction of motion z.
- Which rays, at which angles, are reflected by M1?



• A point on the orbit near the *xz* origin is given by:

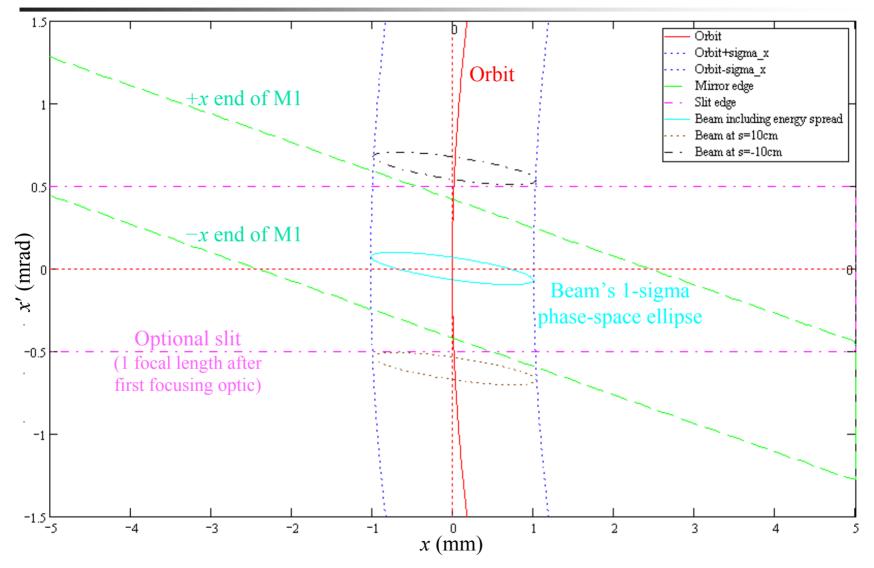
$$(x,z) = (\rho - \rho \cos \theta, \rho \sin \theta) \approx (\frac{1}{2}\rho \theta^2, \rho \theta) = (\frac{1}{2}\rho x'^2, \rho x')$$

- For a point on the orbit, the angle x' to the z axis is equal to θ .
- The rays striking the +x and -x ends of M1 are given by:

$$x + x' \left(z_m \pm \frac{L_m}{2} \cos \alpha_m - z \right) = \pm \frac{L_m}{2} \sin \alpha_m$$
$$x + x' z_m \approx \pm \frac{L_m}{2} \sin \alpha_m$$

• We plot these curves in phase space, along with the beam's 1sigma ellipse at three points along its orbit.

Horizontal Phase Space: PEP-II HER



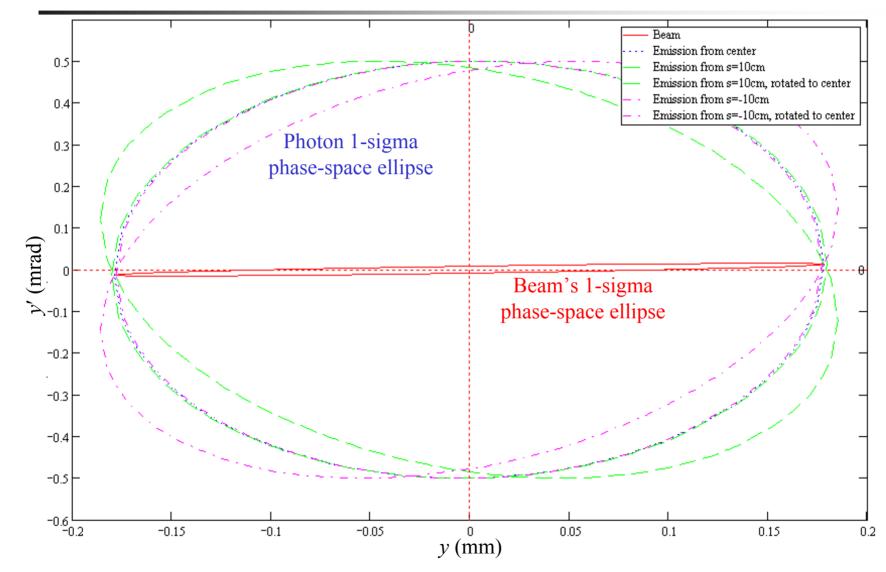
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Fisher — Imaging with Synchrotron Light



- Two source of vertical angle for the light rays:
 - The opening angle σ_{ψ} of each electron's emission
 - The electrons' phase space, which gives each electron its individual angle to the *z* axis
- Compare to the horizontal axis:
 - Only the phase space matters: each electron emits along the tangent to its orbit.
- The opening angle is by far the bigger contributor.

Vertical Phase Space: PEP-II HER



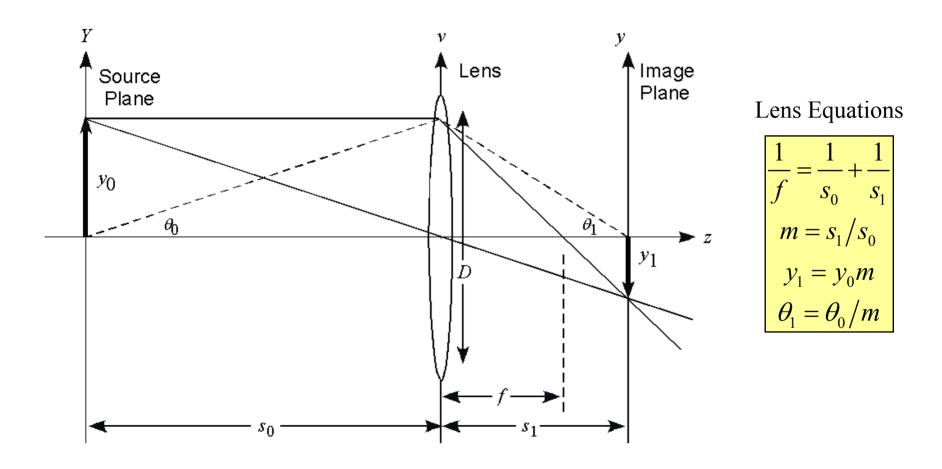
Fisher — Imaging with Synchrotron Light

- Accelerator people know that Liouville's theorem conserves the emittance of a beam in a transport line.
 - The phase-space ellipse changes shape, but not area.
 - At each waist, the size-angle product $\sigma_x \sigma_{x'}$ is constant.
 - (But in a ring, dissipation by synchrotron radiation allows damping that "cheats" Liouville.)

• Light in an optical transport line has an emittance too.

- At each image, the product of size and opening angle (light-cone angle) is constant.
 - Magnification makes the image bigger, but the angle smaller.
- The area of the light's phase-space ellipse—the brightness of the source—is conserved.





- The minimum emittance for a light beam is that of the lowest-order Gaussian mode (TEM_{00}) of a laser.
 - ω is the beam radius.
 - In the usual definition (where ω is not the one-sigma value):
 - The electric field follows $E(r) = E_0 \exp(-r^2/\omega^2)$
 - The intensity (power) is the square: $I(r) = I_0 \exp(-2r^2/\omega^2)$
 - ω_0 is the radius at the waist (the focus).
 - This size is nonzero due to diffraction.
 - $z_R = \pi \omega_0^2 / \lambda$ is the Rayleigh range.
 - Characteristic distance for beam expansion due to diffraction.
 - The expansion is given by $\omega^2(z) = \omega_0^2 (1 + z^2/z_R^2)$
 - The angle (for $z >> z_R$) is $\theta = \omega/z = \omega_0/z_R = \lambda/\pi\omega_0$
 - The product of waist size and angle is then $\omega_0 \theta = \lambda / \pi$
 - One-sigma values for the size and angle of *I* give an emittance of $\lambda/4\pi$



- Distance to the first mirror
 - Flush with the beampipe wall?
 - Far down a synchrotron-light beamline?
 - Ports and M1 itself introduce wakefields and impedance.
 - The heat load on M1 is reduced by distance.
- Distance to the imaging optics
 - In a hutch: adds distance to get outside shielding
 - In the tunnel: not accessible, but often necessary for large colliders.
- Size and location of the optical table.



- Choose a source point with a large *y* size, to lessen effect of diffraction.
- Magnification: Transform expected beam size to a reasonable size on the camera.
 - 6σ < camera size < 10σ : Uses many pixels; keeps the image and the tails on the camera; allows for orbit changes.
 - Needs at least two imaging stages: Since the optics are generally far from the source, the first focusing element strongly demagnifies.
- Optics: Use standard components whenever possible.
 - For example, adjust the design to use off-the-shelf focal lengths from the catalog of a high-quality vendor.
 - Use a color filter to avoid dispersion (or use reflective optics).
 - Correct the focal length (specified at one wavelength) for your color.



- You can iterate a lot of the basic design in a simple spreadsheet.
 - Enter the fixed distances.
 - Specify the desired magnifications.
 - Solve the lens equations, one stage at a time, to find lenses giving the ideal magnifications.
 - Change the lenses to catalog focal lengths.
 - Correct their focal lengths (using the formula for each material as found in many catalogs).
 - Adjust magnifications and distances.